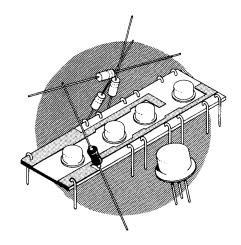


Handling and Selection Guide



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Introduction

In 1948, Bell Telephone Laboratories scientists announced a tiny new device which was destined to change the world of electronics. Called the transistor, its ever growing family of solid state devices is already providing greatly improved telephone service and offers the promise of many more exciting developments in the future.



Success of the telephone system is dependent upon devices having high reliability at a reasonable cost. Reliability results from good design,

controlled manufacturing processes, and wise selection and handling of the devices.

The active region in a miniature electron tube is approximately a million times greater than the volume of the active region of a typical switching transistor. An appreciation of this scale difference is important in translating conventional electron tube practices to solid state devices. The key to obtaining stable electrical characteristics in a transistor or diode is a surface cleanliness of semiconductor material junction to an atomic level. Maintaining this cleanliness over a very long period of time is the function of the device package or surface passivation.

The device user must therefore appreciate the minuteness of the active region, the cleanliness level established by the manufacturer and the importance of protecting the soundness of the package seal. Lack of such appreciation can lead to degradation of the essential built-in reliability and to the possibility of placing potential defects into circuits doomed to fail in service.

Solid state devices on which our present and future telephone systems are so greatly dependent are expected to operate reliably for many decades. However, a very small percentage of these devices could have a limited life because of improper manufacture or use. These are of great concern because they limit the ultimate reliability of the system in which they are used.

It is the purpose of this book to help the user protect this reliability by setting forth suggestions for the handling of the various solid state devices and making the user more knowledgeable of the devices and why they were selected for their particular application.

Device Description

INTRODUCTION

After World War II, the Bell Telephone Laboratories at Murray Hill, New Jersey, applied considerable effort to the development of a solid state amplifying device using semiconductor materials such as germanium and silicon. It was known in the mid-forties that such materials possess mobile carriers of charge that move under the influence of an electric field resulting in a current. It was also known at this time that two different types of carriers were possible. For example, germanium and silicon atoms possess 4 electrons which could combine chemically, (valence of 4). If some of their atoms were replaced by atoms that have a valence of 5 (for example, phosphorous or antimony). then the extra electrons would be loosely held in the crystal and be relatively free to move about. This forms the n-type crystal. If some atoms of the semiconductors were replaced by a valence three element such as aluminum or boron, then within the crystal structure electrons would be missing. These are called holes which are easily filled by electrons from neighboring atoms. In the process of filling a hole, a new one is created. This process can take place in particular directions depending upon the applied voltage and thus form a current of positive charge. The semiconductor doped in this manner is called p-type.

Early experiments attempted to change the conductivity of a doped semiconductor by the action of a charged plate immediately above its surface. This is similar to the familiar electroscope or cat's fur experiments in elementary physics. It was hoped that a little power on the plate could control considerably more power by changing the conductivity of a semiconductor bar. The results with the charged

plate were insignificant but by trying to increase the effect of the field using points instead of plates, the point contact transistor resulted when one of two points, as shown in Figure 1, was "formed" by the passage of current. As was later proved, the phosphorous in one of the point contacts was the important ingredient for collector operation and hence amplification.

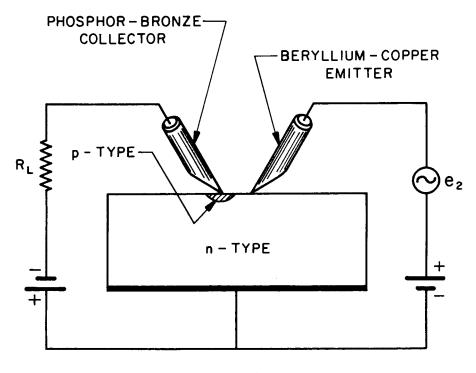
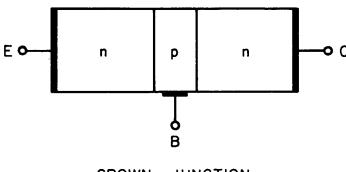


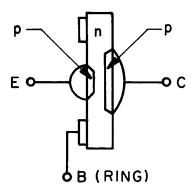
Figure 1.

As a result of the experience gained from the point contact transistor and from a better understanding of junctions formed by n- and p-type regions, the junction transistor was developed two years later. Figure 2 shows the two junction-types which were developed at this time.

DEVICE DESCRIPTION



GROWN JUNCTION



ALLOY JUNCTION

Figure 2.

One type was grown by pulling a seed crystal out of a pool of molten semiconductor material which was alternately doped by n and p impurities. The other was alloyed by melting metal buttons on alternate sides of a wafer and doping the crystal in the resolidification process.

Although point contact transistors remained superior in frequency responses, these junction devices had definite advantages in that they were capable of handling larger power, were less noisy, were easier to handle in circuits, and had a more controllable manufacturing process.

Even though solid-state diodes have a much earlier history, going back before the turn of the century, the invention of the transistor led to a parallel improvement and development of the diode art. This naturally resulted from the intensive effort which went into the better understanding of device physics and materials, and the development of fabrication techniques. Since the diode, with the exception of special types such as the tunnel diode, the gold bonded diode, the regulator diode etc., is essentially a device possessing only two of the three regions of a transistor, it will not be treated as a separate device in this section.

The mid-fifties proved most important in the history of the transistor. In 1955, the diffusion technique was introduced in the junction transistor fabrication process. Thus, under the application of a gas or surface deposition of materials possessing proper impurities, doped regions were formed by the application of heat. These regions which can be controlled to a depth of less than ten billionth of an inch, then allowed for junction transistors to enter the 100 to 1000 megacycle range. The diffusion technique not only led to a break-through in the frequency response of junction transistors but also introduced a batch-type process which was to become the basis of modern transistor technology. Thus, thousands of transistor elements are handled simultaneously through most of the processing reducing greatly the need for individual operations. This also allows for greater uniformity in the product. Figure 3 shows a cutaway section of a diffused base mesa transistor element.

The next significant improvements took place at the end of the fifties with the introduction of the planar epitaxial transistor, as shown in

DEVICE DESCRIPTION

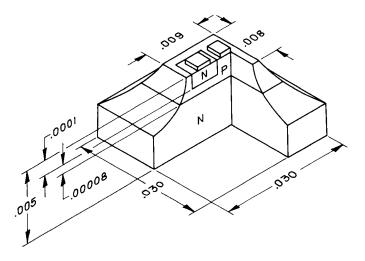


Figure 3.

a cutaway representation in Figure 4. By growing the desired crystal on a heavily doped substrate, as shown by the n_+ region, an improved device, particularly for switching applications is formed. The new

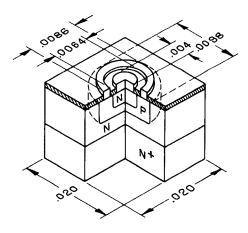


Figure 4.

structure allows for many improvements, particularly higher voltages while still retaining the desired low "on" voltage and switching times.

The planar technique, which eliminates the older mesa formation, also permits close control and reproducibility of junction regions through photographic techniques. The planar structure (i.e., the top surface being flat or planar) also eliminates the problem of interconnections between active elements in the same slice; this was important to solid integrated circuits which soon followed.

Figure 5 shows a monolith integrated circuit using beam leads. Interconnections are made by the "batch process" of evaporation. Thus, good designs and process controls yield circuits which can be made at lower cost than their counterparts using individual components.

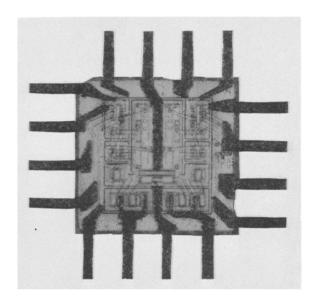


Figure 5.

DEVICE DESCRIPTION

A device giving promise of low cost and good performance, the "Beam Lead" transistor was introduced in the mid-sixties. A single beam lead device is shown in Figure 6.

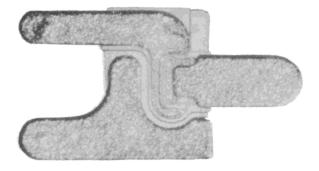


Figure 6.

These devices possess protective coverings across critical boundary regions as well as heavy leads which facilitate the connection problem. The appearance of the relatively thick leads led to the name of "Beam Lead". In order to prevent harmful results of scratches and dust, a relatively simple enclosure can be provided.

Another solid state technique which gives promise of large usage in the Bell System is Thin Film Circuitry. By the use of the refractory metal tantalum, capacitors, resistors and interconnections are all produced in a single pattern on smooth glass or ceramic substrates. With the application of semiconductor devices in the form of Beam Leads, single components or integrated circuits, the circuits which are formed are reproducible and low in cost because of processing which is dependent mainly on photolithographic batch techniques. Figures 7 and 8 show hybrid thin-film circuits using conventional transistors and integrated circuits respectively. The resistors, whose resistance is dependent upon the length, width and thickness

of the tantalum film are mainly shown by the "meandering" lines in the Figures.

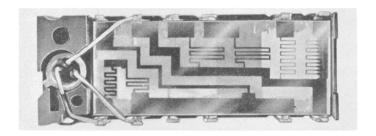


Figure 7.

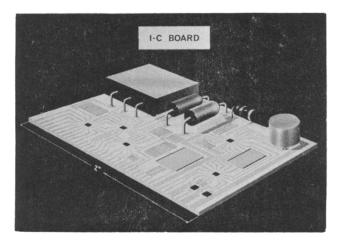


Figure 8.

An interesting review of the historical development which took place in semiconductors and thin films is shown by the tree in Figure 9. The dates in the figure refer mainly to manufacturing dates and not laboratory models or inventions. Some devices were left out in order to simplify the picture. Another interesting story on the transistor

DEVICE DESCRIPTION

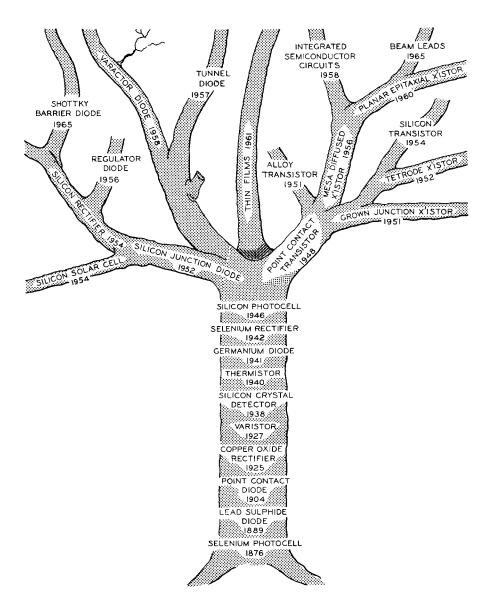
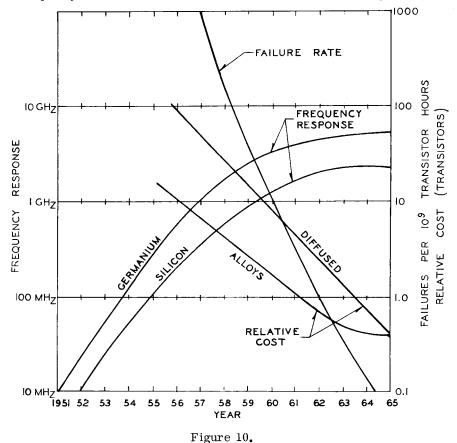


Figure 9.

can be shown by Figure 10 which depicts the improvements which took place through the years in the relative cost, frequency response, and reliability. Germanium has always been ahead of silicon in frequency response because of its higher mobility of charged carriers and partly because it was the first material to be investigated. The



cost picture for diffused devices will continue to decrease as they are incorporated in solid circuits or as beam leaded structures. Alloy transistors should definitely level out as is shown in Figure 10. The reliability curve, which mainly concerns the high-runner logic devices,

DEVICE DESCRIPTION

was based in large part on accelerated testing results. Good agreement has been obtained from results of large systems such as Nike Zeus, Unicom and No. 1 ESS.

Hybrid thin-film circuits, integrated circuits and beam lead devices all have their places in the future. In some areas a number of acceptable alternatives are possible. It is the mutual responsibility of the circuit designer and the device designer to understand the advantages and limitations of the various technologies and to make a choice based upon the best interest of the Bell System.

CHARACTERISTICS

The purpose of this section is to review in general the characteristics, ratings, and reliability which must be considered in selecting transistors for specific applications. Diodes, in general, would follow similar considerations and, therefore, will not be treated separately.

In general, electronic circuits can be classified into switching or analogue applications. A circuit is called upon to recognize the presence or absence of signals and transmit them at higher levels or recognize various levels and phases of signals and amplify them accordingly. Some applications such as high level amplifiers, mixing, etc., could fall into both categories as well as not be considered at all in these general applications. The differences in the two circuit applications are reflected in the requirements of the transistors. Transistors are specified according to their ability to operate as a switch or as an amplifier. In switching applications dc gain, "on" voltage, "off" voltage, input voltage, high frequency response and storage time, play dominant roles. In amplifying applications, the high frequency response, the power gain, power dissipation, input impedance, and noise figure contribute significantly. In any case, a transistor can be optimized for a particular application. The type of structure (epitaxial or non-epitaxial), horizontal and vertical

geomtery, and levels of impurity doping contribute greatly to the optimized design.

Figure 11 shows some of the wafer geometries in our present Bell System devices. It can be seen that the 800 mc transistors, the 44A or 45A type, have a base width W of only about one-fifth that of the 200 mc 16-type. This base width is most important in determining frequency response.

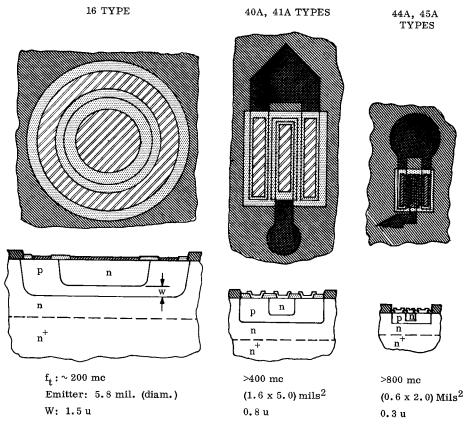


Figure 11.

By paralleling devices internally or redesigning structures by using interdigitation, stars, oak leaves, etc., emitter parameters are in-

DEVICE DESCRIPTION

creased yielding higher current capability without appreciable loss in frequency response.

SPECIFICATIONS AND DATA SHEETS

The objective of the specification is to assure that the product will satisfactorily function in the circuit. A single specification can guarantee performance, in many cases, in several circuits. The specification must not only assure operation at the beginning but also over the desired life of the equipment and over all necessary ambient conditions. Specifications are prepared for the use of manufacturing locations and data sheets for users. Data sheets supply characteristic curves and data that aid in the designing of circuits. The specification states manufacturing and testing requirements which control the quality of the product and provide the most economic balance of manufacturing and testing control to assure proper performance.

There is little doubt that the cost of manufacture and maintenance is of prime importance to every system designer. It is apparent that minimum costs will be achieved when the specification represents the optimum balance between system requirements, device design, and manufacturing skill. A weakness in any of the three areas can but add to the cost of the system. A mutual understanding between the three areas can greatly help in preventing unnecessary costs.

Some of the important considerations which follow a system from initial development to final manufacture and are necessary for optimum cost are the following:

a. Limit values on test specifications and data sheets must not only reflect temperature and aging variations but must also represent a balance between circuit complexity and performance and maximum device yield. Obviously, limits which are too tight increase costs

by increased testing or reduced device yields, while excessively loose limits increase costs by reduced circuit efficiencies.

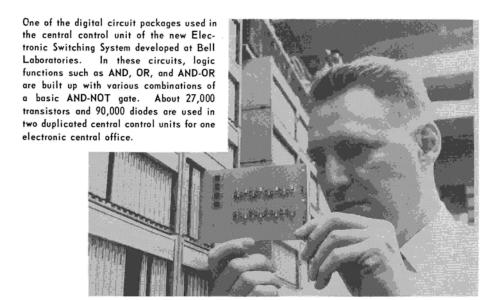
b. Device designs should reflect the latest achievable in electrical performance, reliability, and manufacturability. This can best be obtained by maintaining the areas of design and manufacture at the highest technical level possible and by a constant interchange of information and ideas on new and important product developments and system requirements.

RATINGS AND RELIABILITY

A rating is, by definition, a limit value for a device which if exceeded will impair the expected life of the device. In some cases, the failure can be catastrophic and take place immediately. This generally happens when voltage ratings are exceeded. In other cases the increased degradation will not be immediately apparent but eventually will result in a higher failure rate. This usually results when junction temperature ratings are exceeded.

Handling

With the ever increasing numbers of solid state devices used in today's electronic equipment it is essential that proper handling techniques be employed to insure the overall reliability of the equipment in which they are used. It is the intent of this section to provide these proper handling techniques for the assembly or replacement of solid state devices in such equipment.



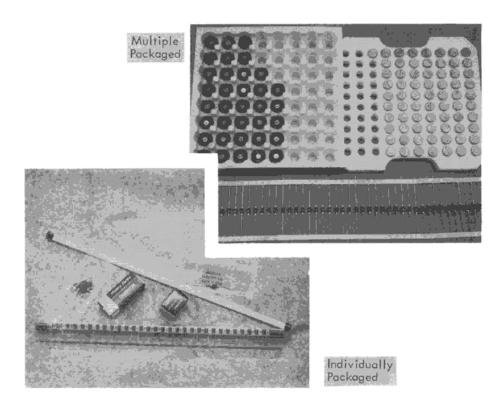
STORAGE

Solid state devices should be stored in their shipping containers whenever possible. These containers are specially designed to give the kind of protection needed. Devices should never be dumped from their cartons into bins. This may result in mechanical shock, cracked glass seals resulting in electrical degradation, and bent or tangled leads, or even

scratched leads which are susceptible to corrosion, making soldering difficult. Integrated circuits and hybrid thin film circuits are even more susceptible due to their construction and multiplicity of components. In cases where devices are provided with additional parts, such as lead spacers, mounting washers, thin film insulators and the like, store them with the device to insure their intended use. In general all devices should be used on a "first in - first out" basis. Prolonged storage may cause oxides to form on the leads, necessitating special cleaning before soldering.

PACKING AND UNPACKING

Semiconductor devices may be received packaged in a number of ways depending on the device requirements, manner in which they will be



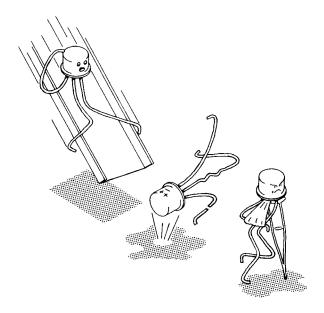
HANDLING

used, or even the number ordered. To insure proper packing the devices should be ordered by specifying standard multiple packaging where possible with the remainder individually packaged. For interworks - locations employing automatic insertion equipment, lead tapes for varistor and diodes and plastic slides and styrene belts for transistors are or will be available. For further information contact the packaging engineer at the producer location. Other bulk packages such as polystrene and styrene vacuum formed Handler-Shipper trays are available. Distributing houses can either order the latter type or in the case of field replacements, individual packaged devices.

If lots must be broken, each group should be repacked in a manner similar to that of the original packing.

MECHANICAL DAMAGE

Semiconductor devices should be handled with about the same care as a glass electron tube if the built in reliability is to be assured. Rough handling or dropping may cause leaks or cracks in the glass seal, damage to the internal wafer (or substrate in the case of thin film circuits), or openings in small internal wire bonds. Although these effects of jolts and jars may not be immediately apparent, they may shorten the life expectancy by causing potential defects. If mechanical damage, such as cracks in the glass seals or substrate, dents in the can (especially the flange), or nicks in the tabulation, is noted, it is recommended that the device not be used. Since thin film circuits are not encapsulated, care must be exercised to avoid damage to the thin film elements. A minute scratch could result in a serious circuit damage. In some cases beryllia is used for mounting washers or device piece parts because of its good heat-conducting and poor



electrical-conducting properties. Care must be exercised in handling this material since it is known to be toxic.

In general, solid state devices are capable of withstanding shocks of the order of 2000g. A fall from a bench to the floor may produce a shock as high as 6000g, depending on the device, the position of impact, and the type of floor surface. Exposure of a transistor or diode to any single jolt or jar may not result in an immediate failure, but shocks in general should be avoided. Microwave point contact diodes, alloy transistors, integrated circuits and thin film circuits are the most susceptible to shock, due to their internal construction.

HANDLING

LEADS

Most semiconductor devices employ a glass-to-metal-seal. The leads of the devices are made with material such as Kovar and Rodar to match the thermal expansion of glass. The number of bends to which a lead may be subjected should be kept at a minimum to assure soundness of the seal. Forcing leads into alignment with terminals or posts by twisting or pulling may damage the seal. All bends should be made not closer than 1/16 of an inch (unless otherwise specified) from the surface of the glass seal or, in the case of plastic encapsulated devices, from the body of the device. Closer bends can result in cracking of the seal, with deterioration of the enclosed environment resulting in lower reliability of the device. The cracks may not be readily apparent even under a microscope.

Bent and tangled leads caused by improper handling may result in slow leaks developing in glass seals, or in broken leads or structural changes that would initiate stress corrosion. Handling of leads should be kept to a minimum, as residues from body oils are likely to cause soldering difficulties.

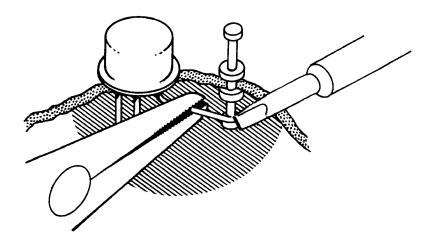
Improper cutting of semiconductor device leads (such as with diagonal pliers), can result in a mechanical shock wave which may travel through the lead into the device and degrade its electrical properties. A shearing tool should be used to minimize the possibility of shock damage. Shears of roughly the same size as diagonal pliers are commercially available and are preferred.

The wirewrapping of semiconductor device leads requires special consideration because of the residual tension and the stress corrosion effects which may develop. This is especially true of gold-plated Kovar or Rodar leaded devices. It is recommended that the appropriate Bell Laboratories Applications Group be consulted before wirewrapping of semiconductor device leads is undertaken. The use

of percussion welding is generally not recommended for semiconductor devices, because of the likelihood of damage due to the high currents generated. Resistance welding may be acceptable, provided care is taken to insure that no destructive transients are introduced into the devices. This is particularly applicable to devices which usually have one element connected to the case. Low-power devices, such as ultra-high frequency and NPN alloy transistors, are especially susceptible. The appropriate Bell Laboratories Applications Group should be consulted in regard to wirewrapping or welding techniques.

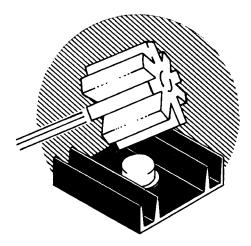
HEAT SINKS

Heat sinks are classified under two types: (1) the temporary type, which is used in soldering to prevent the introduction of excessive heat to the semiconductor device.



and (2) the permanent type, which is installed with the device to allow a greater dissipation of heat generated within the device itself. The latter can be either a radiator fin-type, which surrounds and is part of the device, or the external type which is mounted to the stud of the

HANDLING



device during circuit assembly. The temporary type will be discussed in the following section on Soldering.

From the electrical standpoint, permanent type heat sinks are used to reduce junction temperature for increased power dissipation capability and reliability. The ability of a semiconductor device to dissipate its rated power is dependent upon (1) internal thermal resistance of the device itself and (2) external factors, such as the size of the heat sink, the thermal resistance between the heat sink and the device, the degree of ambient circulation, and the temperature of the ambient. Device data sheets often contain information concerning these external factors.

The bearing surface upon which a stud-mounted semiconductor device is installed must be flat, clean and free of burrs. This is necessary to insure adequate contact between the heat sink and the device in order to obtain proper heat flow. Thermal contact is improved with a very thin film of silicone lubricant between the clamped surfaces. Care should be used to insure the torque recommended in the data sheets. When electrical isolation is required between the device and an external

heat sink, a thin mica or other suitable washer, coated with silicone lubricant, can be used between the two. Care must be taken not to damage the insulating washer.

SOLDERING

A soldering iron, properly connected and grounded may still have leakage voltages present on its tip in excess of 1 volt above ground. This voltage can cause damage, particularly to ultra-high frequency transistors which have emitter-to-base breakdown voltages in the range of 1 volt. With such devices, it is desirable to use a working surface isolated from ground. Some soldering guns, even when adequately grounded, produce transient voltages each time the power is turned on or off. These are caused by the inductive reactance in the tool and ground lead. Particularly susceptible to damage from these transients are NPN germanium alloy transistors, ultra-high frequency transistors, and microwave point-contact diodes.

Wave and dip soldering have an advantage over hand soldering because the entire circuit board is maintained at the electrical potential of the molten solder. Thus, destructive transients are not introduced into the devices. Care must be exercised to insure that solder bath temperatures are uniform, that the duration of immersion is timed properly, and that the devices are not immersed closer than 1/16 of an inch from the glass-to-metal seal. In the case of thin film circuits, time and temperature must be properly controlled to prevent damage to previously soldered connections. Failure to follow these precautions can result in small changes in electrical characteristics which are not easily detected, but which may cause failure of the device. The length of time to which a semiconductor device may safely remain in the molten solder is dependent upon the type (whether alloy or diffused), the temperature of the bath, and the distance heat must flow to reach the critical areas of the device.

HANDLING

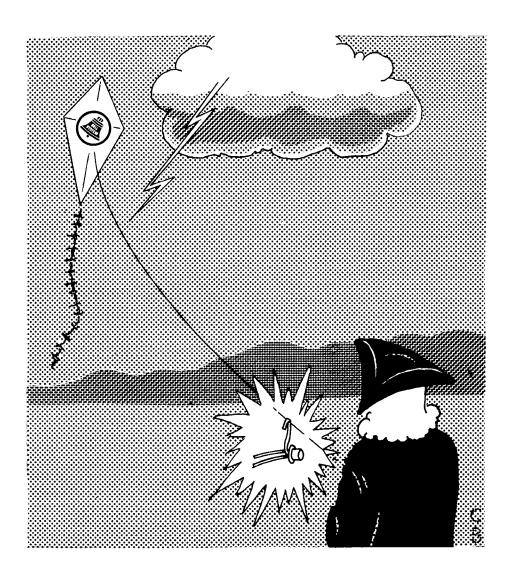
Following are some additional recommended practices to use when soldering solid state devices:

- 1. Higher solder bath temperatures for a shorter time are preferred for better solder-wetting of the leads, and to prevent long heat exposure from affecting the critical areas of the device.
- 2. Corrosive fluxes should not be used to facilitate soldering.
- 3. Diffused type devices can withstand higher temperatures for longer periods of time than can alloyed types which use lower temperatures in processing. As an example, diffused transistors of the 15- or 16-type families can withstand a 575°F bath for a period of 1 minute when immersed to not more than 1/16 of an inch from the seal. The 12-type germanium alloy transistor should not exceed 460°F in the same bath for more than 30 seconds. In hand soldering, somewhat higher iron tip temperatures can be used if only one lead is heated at a time. For example, with the 12-type germanium transistor the temperature of the iron tip should not exceed 930°F at a minimum distance of 1/16-inch away from the seal for a short duration.
- 4. Resoldering of thin film circuits should be avoided since local stresses may be developed, resulting in cracked substrates.
- 5. Any soldering information which may be included in the device data sheets should be followed.

STATIC CHARGES AND TRANSIENTS

A static charge of several thousand volts can easily build up on your body from simply walking about on a nonconductive floor, or moving around in a chair. This is particularly true in low humidity, and when clothing made of wool or certain synthetic fibers, such as nylon, is worn. Ordinarily, this static charge may be high enough to send a damaging pulse through a semiconductor device when it is touched. Before handling ultra-high frequency transistors, milliwatt NPN germanium

alloy transistors, and microwave point-contact diodes, be sure to ground static charges by touching some grounded metal object, such as the metal work bench. In extreme cases, sensitive devices may require handling in a completely shorted condition, and operators may require special grounding facilities.



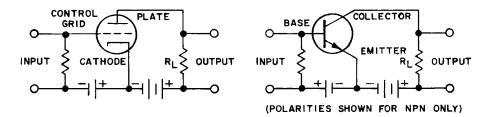
HANDLING

Electric tools, such as screwdrivers and wirewrappers, are frequently used in the assembly of circuit boards containing semiconductor devices. Some devices can be damaged by transients generated by these tools. Air-operated tools are recommended for working on circuits employing ultra-high frequency transistors, milliwatt germanium NPN alloy transistors, microwave point-contact diodes, and epitaxial devices.

BLANK

Electrical Testing

The long established procedures and equipment for testing electron tube circuits do not directly apply to circuits using semiconductor devices. This is true because parameters are greatly dependent on temperature and strict limits exist on the upper values of applied voltage. If voltage limits are exceeded an abrupt change in impedance may take place which usually results in damage unless the circuits are designed to limit the current.



TUBE-TRANSISTOR ANALOGY

CIRCUIT TESTING

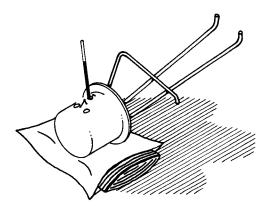
Performance tests on completed circuits must be made in such a way that ratings will not be exceeded for even very short periods of time. Exceeding these ratings may cause a sudden, permanent change of characteristics or may start a long slow change resulting in eventual circuit failure.

Transient energy in the form of voltage spikes or current surges may be generated when sudden changes occur, such as turning a circuit on or off. Similar effects are produced by momentary shorts in live circuits or connection of a low impedance probe for troubleshooting.

These undesirable transients may exceed the maximum ratings of devices in the circuit and cause damage. Caution should be used to prevent or minimize their occurrence.

It is good practice to turn off the power when connecting or removing circuit boards from a test set. In some cases, it may be necessary to short the test set connector terminals in order to discharge the energy stored in wiring and other capacitance in the test set, even though all power supplies are disconnected.

After all necessary connections are made and test set connector short circuits removed, test voltages can be applied in a particular sequence. The BTL circuit design engineer can provide this sequence.



Consideration must be given to ambient temperature when testing solid state circuits, since some semiconductor device parameters can undergo a 2-to-1 change when the temperature is changed as little as 10° C.

Following the operating tests, all voltages should be returned to zero in a proper sequence. In the special case mentioned previously, the test set terminals must be shorted before the circuit under test is removed.

ELECTRICAL TESTING

Devices particularly susceptible to test set transients are microwave point-contact diodes, ultra-high frequency transistors, and germanium NPN alloy transistors.

CIRCUIT TROUBLESHOOTING

When it is necessary to troubleshoot and repair an assembled circuit which does not operate properly many approaches can be taken. It is not within the scope of this book to define methods of locating defects, but rather to offer precautionary suggestions which may apply.

"Buzzers" of the electromechanical type, often used as continuity testers, are prolific generators of high-energy transients. Destructive transients may be developed, even though the buzzer battery voltage is much lower than the normal voltage applied to the circuit under test. For this reason, such "buzzers" should never be used when trouble-shooting circuits containing semiconductor devices.

Wiring continuity tests can be made safely by use of a selected ohmmeter or electronic buzzer, that is, one that does not exceed the current or voltage ratings of the devices in the circuits being tested.

Typical ohmmeters and a special "Buzzer" developed at Western Electric, Omaha are compared in the following table:

TYPICAL OHMMETER DATA

Description	MAX SHORT CIRCUIT CURRENT (Low Ohm Scale)	MAX OPEN CIRCUIT VOLTAGE (High Ohm Scale)	MAX POWER TO DEVICE UNDER TEST
Omaha "Buzzer" SID 321011	1 MA	0.5 Volts	0.25 MW
Triplett Model 630-L X1 and X10 X1K and X100K	12 MA 0.34 MA	0.14 Volts 34 Volts	0.42 MW 0.68 MW
Hewlett-Packard Model 412A	10 MA	1 Volt	2.5 MW
Simpson Model 260	140 MA	7.5 Volts	30 MW
Triplett Model 310	80 MA	16 Volts	30 MW
RCA Voltohmyst Model WV-97A	150 MA	1.5 Volts	60 MW
Weston Analyzer Model 980 Mark II	60 MA	4 Volts	90 MW
Triplett Model 630	350 MA	34 Volts	112 MW

Because of its low voltage, low current and limited power the Omaha "Buzzer" is recommended for continuity testing of any circuits containing semiconductor devices. It is always good practice to remove all power to a circuit when an ohmmeter is used. Even though power is removed transients can result from connecting or disconnecting an ohmmeter

ELECTRICAL TESTING

across a transformer winding or other inductive element. Damage to a semiconductor device in an adjacent circuit may result.

Troubleshooting by bias measurement or signal tracing is, of necessity, performed with power on. Connecting or disconnecting test probes may cause damage to a semiconductor device by transients because of the effects of their low impedance or high input capacitance. Probe input capacitances may become charged at one point in the live circuit and then, at the next point of application, discharge destructive energy through a semiconductor device. The practice of using high impedance probes and, if necessary, shorting between readings will eliminate this problem.

Improper grounding may cause leakage currents from ac-line-operated test equipment, which will result in damage to devices in the circuit under test.

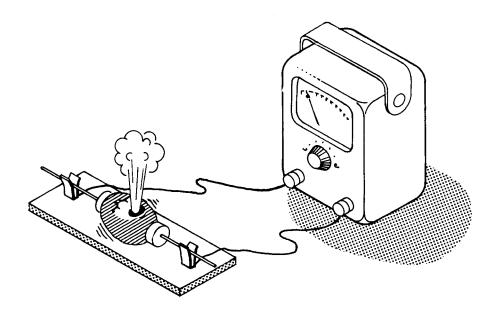
High voltage static charges which build up on clothing, particularly in low-humidity environments, may be injurious to some low-power semiconductor devices if discharged through them. This can be easily avoided by touching a grounded metal object before handling a semiconductor circuit. Use of conductive flooring and the wearing of suitable clothing and shoes may also be employed to prevent the build-up of static charges.

DEVICE TESTING

Transistors and diodes can be tested as individual units by removal from the system or while wired into a circuit. <u>Precautions should be followed to avoid exceeding the device ratings as described in the sections on Circuit Testing and Troubleshooting.</u>

Several general-purpose transistor and diode testers are available commercially which will measure several of the functional parameters. Tests of dc parameters such as leakage current, breakdown voltage and

current gain (of transistors) will indicate the normal type of failures such as opens, shorts or appreciable degradation since it was thoroughly tested by the manufacturer. (The Hickok Model 870 is a typical example of a commercial tester.)



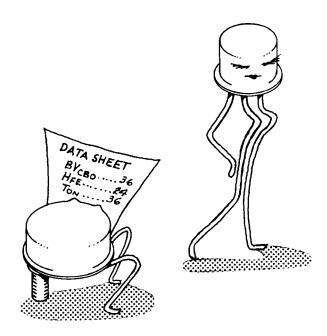
In some instances an ohmmeter may be used to indicate opens or shorts. Any tester selected should be checked by the user to assure that it does not apply voltages or currents exceeding the ratings of the device being tested.

A common method of making a quick check of a semiconductor device or thin film circuit believed to be dynamically defective is to insert it into a circuit or system known to be in working order. All power to the circuit should be removed before inserting the "doubtful" device to reduce transients. In some circuits it may also be necessary to discharge circuit capacitances in order to eliminate harmful transients before inserting devices. A device known to be good should never be

ELECTRICAL TESTING

placed into a defective circuit since the device itself may be damaged. Units suspected of dynamic failure should be brought to the attention of the device manufacturer.

When testing a semiconductor wired into a circuit, refer to the precautions listed for Circuit Testing and Troubleshooting. There are several commercial "in-circuit" testers available, (such as the Hickok Model 890) which can make limited checks without removing a device soldered into the circuit.



Some device parameters are extremely dependent upon the temperature or bias conditions. Leakage currents may double when the temperature is increased about 10°C. Transistor current gain (common emitter) may vary more than 2-to-1, as the emitter current is varied within the ratings of the device. Consult the device data sheets for proper temperature and bias conditions when testing to specification limits.

BLANK

Failure Classification

INTRODUCTION

Complex electronic system reliability is determined by the reliabilities of the various devices and parts used. Intrinsic device reliability is obtained through good design, processing and controls. Essential to this stability is purity to an atomic level and an encapsulation or package to hold the environment of the active element constant with time.

The user can appreciably lower the intrinsic reliability through excessive exposure to thermal, electrical or mechanical conditions. Disastrous results may be caused by test set transients, improper switching sequences, inductive surges, power line leakage currents, static discharges, capacitance discharges, and troubleshooting equipment and techniques, by overloading the device junction for a brief instant. The effect of energy concentrated in a small volume is a rapid rising temperature (a hot spot), which alloys through causing an electrical short. On occasion the very fine connecting wires are vaporized causing an open.

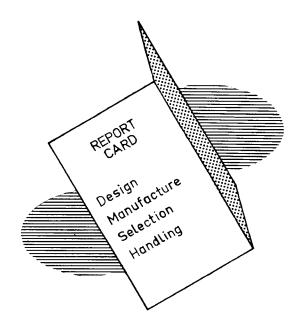
The integrity of the seal and the can may be degraded by shock or stress due to mishandling. A lead bent close to a very thin metal-to-glass seal, or shock transmitted by lead clipping or pulling, may initiate a slow leak and destroy the balance of gases, and purity levels. A relatively slow leak will cause a device to show up in time as a field failure.

CATEGORIES

Failures, in general, are classified into four categories:

1. Device Design - Failure to meet reliability design objectives.

- 2. Device Manufacture Improper device <u>manufacturing</u> techniques and workmanship.
- 3. System Design Incompatability between device <u>selection</u> and equipment specification.
- 4. System Manufacture or User Improper techniques in <u>handling</u> and assembling devices into circuits and systems.



It is important and economical to establish a system to recognize the symptoms and understand the causes of failure so as to assign the failure to the proper category when it occurs in a system or sub-assembly. By proper analyses at the location of the system manufacturer or user (distributing house), made by an expert who is properly trained for the task, many of the failures can be effectively analyzed, and corrective action taken in the shortest possible time. Experience has shown that during the early system testing period

FAILURE CLASSIFICATION

of a new device most failures have resulted from mishandling and improper testing procedures. Since all failures will occur in the system manufacturing or user area, the following steps are recommended:

SYSTEM MANUFACTURE OF USER AREA

- a. Each using area should establish a failure analysis engineer who has been properly trained for this task at Allentown and Reading so that maximum use can be made of the analysis data. He should be thoroughly familiar with device construction, electrical parameters, testing, handling, and known modes of failure. This specialist should perform only the necessary analyses to determine whether the failure was the result of mishandling, testing, and other user operations or the result of a device anomaly. He should also fill in the failure reports, and keep a record of all failures from all assembly lines so as to detect trends and patterns and notify the appropriate "project engineer" (the engineer responsible for the equipment using the solid state devices). Failure analysis reports should be distributed as follows:
 - 1. Reports of failures resulting from mishandling, testing, or other system manufacturing operations should be forwarded to the proper "project engineer" with complete information of the analysis. A copy of this report should also be sent to the Reliability Engineering Organization at the device manufacturing location especially if there are a significant number of such failures.
 - 2. Reports of failures resulting from other causes and the devices should be forwarded to the Reliability Engineering Organization at the device manufacturing location for further analyses and proper action.

b. It should be the responsibility of the project engineer to institute a failure report for each semiconductor device failure. This report should contain complete information, such as the conditions that existed at the time of failure, other devices that failed at the same time, date code, location of device manufacture, etc. The device and the failure report should then be forwarded to the failure analysis engineer. The "project engineer" should also be responsible for taking corrective action where necessary as dictated by the information fed back by the failure analysis reports.

RECOMMENDED AIDS FOR THE FAILURE ANALYSIS ENGINEER

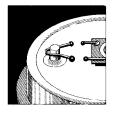
- a. Tektronix Type 575 Transistor Curve Tracer or equivalent for electrical analysis.
- b. De-canning Tool for Autopsy C-694276 (Allentown drawing) or C-732259 and C-732273 (Reading drawings) for opening enclosures.
- c. Microscope Holding Fixture C-732134 (Reading drawing) for ease of visual inspection.
- d. Chart of possible symptoms and causes of semiconductor device failure. (The symptoms are shown for particular geometries, however, they apply equally well to the various geometries which are used for solid state devices.)

FAILURE CLASSIFICATION

SYMPTOMS

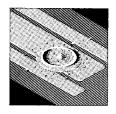
POSSIBLE CAUSES OF FAILURE

Balls on ends of open wires



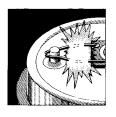
Excessive current or voltage

Fused spot on wafer



Excessive current or voltage

Vaporized wire



Excessive current or voltage

Discoloration of wire or wafer and device shorted

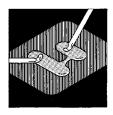


Excessive current or voltage

SYMPTOMS

POSSIBLE CAUSES OF FAILURE

Fused streak across wafer or spike between stripes



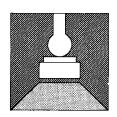
High voltage or static discharge

Wire lifted from stripe



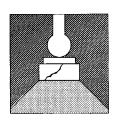
Poor wire bond
Excessive mechanical shock

Wafer off header



Poor wafer bond
Excessive mechanical shock

Cracked wafer



Severe shock

FAILURE CLASSIFICATION

SYMPTOMS

POSSIBLE CAUSES OF FAILURE

Fractured wire at bond or weld



Poor bond or weld

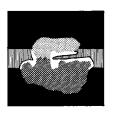
Excessive vibration

Fractured end of wire at Al stripe. Purple color present near wire



Migration of gold from wire to Al stripe sometime called "purple plague"

No observable defect, but device is shorted internally



Static discharge, high voltage pulse, or contamination

Particle or thread like foreign material across junction area

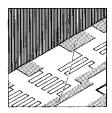


Physical defects due to poor assembly practices

SYMPTOMS

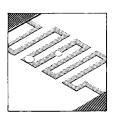
POSSIBLE CAUSES OF FAILURE

Open or high resistance



Scratch due to rough handling

Open or high resistance



"Pinhole" due to manufacturing defect

Open or high resistance.
Broken substrate



Cracked substrate due to shock

Device Characteristics

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15D	Transistor	52	16H	Transistor	52
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483A	Multiple Diodes	72	N4	Thin Film Circuit	77
484A	Multiple Diodes	72	N5	Thin Film Circuit	77
484B	Multiple Diodes	72	N6	Thin Film Circuit	77
485A	Rectifiers	59	N7	Thin Film Circuit	77
485W	10 Watt Volt. Reg.	60	N8	Thin Film Circuit	77
485Y	10 Watt Volt. Reg.	60	N9	Thin Film Circuit	77
486A	Ge Backward Diode	s74	N10	Thin Film Circuit	77
487A 487B	Multiple Diodes Multiple Diodes	72 72	N11	Thin Film Circuit	77

TRANSISTORS

f _T (Med) f _T (Min) ♦ (Mc)	2.6 14.0 1.2	4.2 2.1 2.0 3.3	थ <u>4</u> 4 4 थथ
t _s + t _f (nsec) (Max.)			
td + tr (nsec) (Max.)			
-hfb -hFB (Min.)	0.980 0.968 \$ 0.968 \$ 0.950 0.980 0.970	0.980 0.950 0.950 0.940	0.970 \$0.980 0.980 0.980 0.980
VCE(sus) BVCEV ♦ (Min)	30 + 30 + 30 + 30 + 30 + 30 + 30 + 30 +	10 \\ 35 \\ 45 \\ 25 \\	40
BVEBO (Min.)	20 20 30 30 50	20 20 20 20 20	20 20 20 20 20
ICBO (μAdc) (Max.)	10 10 15 15 300 20 20	10 10 10 10	10 10 10 10
BVCBO BVCES∳ (Min.)	440 330 60 440 40	40 40 40 45 40	40 40 40 40 40
Power (Watts) @ 25 C	0.25 0.25 0.25 30.0 2.80 0.25	0.25 0.25 0.25 0.25 0.25	0.25 0.25 0.25 0.25 0.25
Status	A&M P R P R P	4444	r r r r r r r
Package	9 9 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	9-d 19-6 19-9-0	9-d 19-6 19-6 19-6
Description	Alloy Ge P-N-P Alloy Ge P-N-P Alloy Ge N-P-N Alloy Ge N-P-N Alloy Ge P-N-P	Alloy Ge P-N-P Alloy Ge P-N-P Alloy Ge P-N-P Alloy Ge P-N-P Alloy Ge P-N-P	Alloy Ge P-N-P Alloy Ge P-N-P Alloy Ge P-N-P Alloy Ge P-N-P Alloy Ge P-N-P
Code	7A 7B 8B 8C 9A 9B 9D 12A	12B 12D 12E 12E 12F	12H 12J 12K 12K 12L 12L

P=Preferred Note: Power ratings are for free air operation. All electrical values are "Initial Limits". R = Restricted (Check use with Applications Engineer) *BVCEO ** t_S † hfe †† Epitaxial * hFE

Care should be taken if any of the breakdown characteristics such as BVCEO, BVCES, BVCER are exceeded. This is particularly true of epitaxial transistors which have low collector body resistance.

TRANSISTORS

1	· · · · · ·		7		
	f _T (Med) f _T (Min) ♦ (Mc)	400 ♦	300 ♦ 320 ♦ 350 ♦ 350 ♦ 300 ♦	300 300 300 300	220
	t _s + t _f (nsec) (Max.)	le Max.	200 **	150 **	
	td + tr (nsec) (Max.)	= 3.0 Vc	wng		
	-hfb -hFB ♦ (Min.)	0.960 ♦ †15-330 †30-200 VCE(sat) = 3.0 Vdc Max.	0.970 0.972 0.978 \$ 0.980 0.970 \$	0.950 0.960 0.976 0.968	0.972 0.980 0.952 †43
	VCE(sus) BVCEV ♦ (Min)	65	22 35 12 28	22 28 24 35	35 20 ♦ 15 ♦ 36 ♦
	BVEBO (Min.)	20 0.8) = 1.5 Vd 0.8	0°2 0°2 0°3 0°2	6.0 6.0 6.0 6.0	6.0 10 20 20
	ICBO (µAdc) (Max.)	10 6.0 it VCE(sat 6.0 it NF = 31	0.1 0.1 0.1 0.1	0.03 0.03 5 db NF 0.1 0.03	0.03 1.3 2.9 2.0
	BVCBO BVCES ♦ (Min.)	65 30 15A excep 30 15C excep	60 + 60 + 60 + 60 + 60 + 60 + 60	60	90 ♦ 20 20 38
	Power (Watts) @ 25 C	0.25 0.25 Same as 0.25 Same as	0.40 0.40 0.40 0.40 0.40	0.40 0.40 Same as 0.40 0.40	0.40 0.24 0.24 0.24
	Status	ччччж	A&M A&M P A&M A&M	& & & & & & &	中民民民
	Package	P-6 P-8 P-8 P-8	P-1 P-1 P-1	P-1 P-1 P-1	P-1 P-1 P-1
	Description	Alloy Ge P-N-P Diff, Ge P-N-P Diff, Ge P-N-P Diff, Ge P-N-P Diff, Ge P-N-P	Diff. Si N-P-N	Si Planar N-P-N Si Planar N-P-N Si Planar N-P-N Si Planar N-P-N Si Planar N-P-N	Si Planar N-P-N Alloy Ge P-N-P Alloy Ge P-N-P Alloy Ge P-N-P
	Code	12N 15A 15B 15C 15C	16A 16B 16C 16D 16E	16F 16G†† 16H 16J†† 16K	16L 17A 17B 17C

P = Preferred Note: Power ratings are for free air operation. All electrical values are "Initial Limits". R = Restricted (Check use with Applications Engineer) **BVCEO *** ** † * $^$ **t

ABOVE QUICK SELECTION DATA NOT TO BE USED FOR CIRCUIT DESIGN - USE OFFICIAL DATA SHEET.

Care should be taken if any of the breakdown characteristics such as BVCEO, BVCES, BVCER are exceeded. This is particularly true of epitaxial transistors which have low collector body resistance.

TRANSISTORS

			,	
f _T (Med) f _T (Min) \blacklozenge (Mc)		180 + 180 + 140 + 180 + 200 + 180 +	110 ♦ 110 ♦	180 180 180 180 110
t _s + t _f (nsec) (Max.)		350	009	150
t _d + t _r (nsec) (Max.)	lb max.	150	100	90 85
-hfb -hFB ♦ (Min.)	a NF = 6 \dot{c}	0.962 0.952 0.952 \$ 0.952 0.955	0.952 0.952 ♦	† 27 † 22 † 22 * 25 † 22 0.944 ♦
V _{CE} (sus) BV _{CEV} ♦ (Min)	The product of the two hfe.s is 3200 to 14,000 Same as 18A except one of the two transistors has a NF = 6 db max. The product of the two hfe.s is 3200 to 14000 The product of the three hfe.s is 18×10^4 to 18×10^5	30 22 50 22 30	30 32	30 22 22 30 30 22
BVEBO (Min.)	is 3200 to e two tran is 3200 to s is 18 x 1	7.0 7.0 7.0 7.0 6.0	6.0 6.0	6.0 6.0 6.0 6.0 7.0
ICBO (µAdc) (Max.)	two hfers tone of th two hfers three hfer	1:0000	1.0	0.0 0.5 0.5 0.1
BVCBO BVCES ♦ (Min.)	The product of the two h _{fe's} is 3200 to 14,000 Same as 18A except one of the two transistors. The product of the two h _{fe's} is 3200 to 14000. The product of the three h _{fe's} is 18 x 10 ⁴ to 1.	60	75 + 75	555
Power (Watts) @ 25 C	The proc Same as The proc The proc	1,50 1,50 1,50 1,50 1,50	1.50 1.50	1.50 1.50 1.50 1.50 1.50 0.40
Status	A&M A&M R A&M	A&M A&M A&M A&M A&M A&M	A&M A&M	P P P P A&M
Package	P-7 P-7 P-7	P-73 P-73 P-73 P-73 P-73	P-73 P-73	P-67 P-67 P-67 P-67 P-67
Description	Two 16A's Two 16A's Two 16F's Three 16A's	Diff. Si N-P-N Diff. Si N-P-N Diff. Si N-P-N Diff. Si N-P-N	Diff. Si N-P-N Diff. Si N-P-N	Si Planar N-P-N Olff. Si N-P-N
Code	18A 18B 18C 19A	20B 20C 20D 20D 20E	20G 20H	20J 20K 20M 20N†† 20P 21A

Note: Power ratings are for free air operation. All electrical values are "initial Limits". cations Engineer) **BVCEO **ts † hfe †† Epitaxial **hFE P = Preferred

R = Restricted (Check use with Applications Engineer)

Care should be taken if any of the breakdown characteristics such as BVCEO, BVCES, BVCER are exceeded. This is particularly true of epitaxial transistors which have low collector body resistance.

TRANSISTORS

					_						_						
f _T (Med)	fT (Min) • (Mc)	200 \$	\$ 062									220	220	220	260	220	260
ts + tf	(nsec) (Max.)	40 40		40	40	40											_
td + tr	(nsec)	85 85		85	85	85	•	**150	T = 40 C								
qJ _q _	-hFB ♦ (Min.)	0.970 \$	0.970	★ 27	★ 42-184	★ 31	144-184	* 40	max. at I		mnm	0.972	0.972	0.972	0.975	0.972	0.975
VCE(sus)	BVCEV (Min)	18 22	22	22	18	22	22	24	Difference between the two is 5mVdc max, at		Noise figure of one of the two is 7 db maximum	35	35	35	35	35	35
	BVEBO (Min.)	7.0	7.0	6.0	6.0	6.0	0.9	6.0	ween the t		of the two	7.0	0.9	7.0	7.0	0.9	0.9
ICBO	(µAdc) (Max.)	0.1	0.1	0.03	0.03	0.03	0.03	0.1	erence bet	and hre	ire of one	0.1	0.03	0.1	0.1	0.03	0.03
BVCBO	BVCES (Min.)	09	• 09	09	09	09	09	65	VBE Diffe	Matched for VBF and hFF	Noise figu	• 06	• 06	• 06	• 09	• 06	• 09
Power	(watts) @ 25 C	0.40	0.40	0.40	0.40	0.40	0.40	0.40		Matched		0.78	0.78	0.83	0.83	0.83	0.83
	Status	A&M A&M	A&M	В	R	Я	R	В	A&M	Ъ	A&M	A&M	Д	A&M	A&M	Ъ	Д
	Package	P-71 P-71	P-71	P-71	P-71	P-71	P-71	P-71	P-1	P-1	P-1	P-69	P-69	P-14	P-14	P-14	P-14
	Description	Diff. Si N-P-N Diff. Si N-P-N	Diff. Si N-P-N	Si Planar N-P-N	Two 16A's	Two 16F's	Two 16A's	Diff. Si N-P-N	Si Planar N-P-N	Diff. Si N-P-N	Diff. Si N-P-N	Si Planar N-P-N	Si Planar N-P-N				
	Code	21B 21C	21D	21F	21G	21H	21J	21K	22A	22B	22C	23A	23B	24A	24B	24C	24D††

All electrical values are "Initial Limits" † hfe †† Epitaxial ★ hFE $P={\rm Preferred}$ Note: Power ratings are for free air operation. $R={\rm Restricted}$ (Check use with Applications Engineer) *BVCEO ***t_S *BVCEO Care should be taken if any of the breakdown characteristics such as BVCEO, BVCES, BVCER are exceeded. This is particularly true of epitaxial transistors which have low collector body resistance.

ABOVE QUICK SELECTION DATA NOT TO BE USED FOR CIRCUIT DESIGN - USE OFFICIAL DATA SHEET.

TRANSISTORS

$_{\mathrm{fT}}^{\mathrm{fT}}$ (Med) $_{\mathrm{fT}}^{\mathrm{fT}}$ (Min) $_{\mathrm{Mc}}^{\mathrm{o}}$	009 ♦	350		
t _s + t _f (nsec) (Max.)	ь Мах.	125		
td + tr (nsec) (Max.)	(NF=7.5d @ 70Mc)	75		
-hfb -hFB ♦ (Min.)	20	0.968 \$0.988 \\ 0.980 \\ 0.980 \\	0.988 0 0.980 0 0.980 0 0.988 0	0.980 . 0.0 nsec
VCE(sus) BVCEV ♦ (Min)	Individual NF of two of the five is 7 db maximum 20 5.0 0.8 10 * †15-2	Same as $26A$ except NF = 6.0 db Max. @ 70 Mc Two have h _{fe} 50-100; two h _{fe} 80-200; three h _{fe} 50-200 0.40 35 0.11 6.0 30 0.96 0.40 30 15 30 0.96 0.40 30 15 30 0.99	35 + 40 + 40 + 40 + 40	0.95 30 15 30 \bullet 0.980 Each with $t_{\rm S} + t_{\rm I} = 11$ -38 nsec and matched within 4.0 nsec Each with $t_{\rm S} + t_{\rm I} = 11$ -38 nsec and matched within 4.0 nsec Matched for minimum carrier leak
BVEBO (Min.)	o of the fiv	0 db Max. ie 80-200; 6.0 30	30 40 40 40 40	30 c and matc c and matc er leak
ICBO (µAde) (Max.)	NF of two	ot NF = 6. 10; two hf 10. 15 15	15 10 10 10	15 11-38 nse 11-38 nse um carrie
BVCBO BVCES ♦ (Min.)	Individual 20	Same as 26A except NF = 6.0 db Max. @ 70 Mc Two have hfe 50-100; two hfe 80-200; three hfg 0.40 35 \bullet 0.1 6.0 30 \bullet 0.40 30 15 30 \bullet 0.40 30 15 30 \bullet	30 40 40 40 40	Each with $t_{\rm S}+t_{\rm f}=11-38$ nsec and Each with $t_{\rm S}+t_{\rm f}=11-38$ nsec and Matched for minimum carrier leah
Power (Watts) @ 25 C	0.10	Same as Two hav 0.40 0.40	0.40 0.40 0.40 0.40 0.40	0.95 Each wi Each wi Matchec
Status	A&M P	7	요요요요	P A&M R R
Package	P-1 P-11A	P-11A P-1 P-7 P-13 P-13	P-13 P-13 P-13 P-13	P-9 P-71 P-71 P-6(2)
Description	Five 16A's Diff. Ge P-N-P	Diff. Ge P-N-P Seven 17A's Si Planar N-P-N Alloy Ge N-P-N	Alloy Ge N-P-N Alloy Ge P-N-P Alloy Ge P-N-P Alloy Ge P-N-P Alloy Ge P-N-P	Alloy Ge N-P-N Two 21B's Two 21G's Alloy Ge P-N-P
Code	25A 26A	26B 28A 29A†† 30A 30B	30C 31A 31B 31C 31D	32A 33A 33B 35A

Note: Power ratings are for free air operation. All electrical values are "Initial Limits" \triangle t_S = 15 nsec $^\dagger \mathrm{h}_{\mathrm{FE}}$ # Dual transistor (two wafers in same enclosure) each exhibiting the electrical characteristics given. †† Epitaxial R = Restricted (Check use with Applications Engineer) *BVCEO *** $_{\rm F}$ * bfe $\Phi_{\rm ICES} = 0.06~\mu{\rm Adc}$ **NF = 3.3 db Max. © 70 Mc *** NF = 4.0 db Max. © 70 Mc P = Preferred

Care should be taken if any of the breakdown characteristics such as BVCEO, BVCES, BVCER are exceeded. This is particularly true of epitaxial transistors which have low collector body resistance.

TRANSISTORS

												1
$f_{\mathrm{T}}^{\mathrm{f}}$ (Med) $f_{\mathrm{T}}^{\mathrm{f}}$ (Min) ϕ				• 009	.4.	♦ 008	008	900	9008	006	008	850
t _s + t _f (nsec) (Max.)			15 ▶	l GT								
td + t _r (nsec) (Max.)	20 db											
-hfb -hFB (Min.)	noise test<	0.988	0.968	0.968 ◆ ★50-200	0.970	†40-300	140-300	140-300	140-300	175-300	†75 - 300	175-300
VCE(sus) BVCEV ♦ (Min)	Same as 35A except carrier leak test omitted and noise test<50 db Same as 8B except base lead has compound bend	35 ♦	12	* 10 *	40 ♦	12	12	12	12	16	12	12
BVEBO (Min.)	eak test o	40	5.0	0.4	20	4.0	4.0	4.0	4.0	4.0	4.0	4.0
ICBO (μAde) (Max.)	t carrier l base lead	09	0.03	0.00 2.0	10	0.01	0.01	0.02	0.04	0.08	0.02	0.04
BVCBO BVCES♦ (Min.)	Same as 35A except carrier leak test omitted an Same as 8B except base lead has compound bend	40	25	► 62 20	40	21 💠	21 🛊	21	21	21	21 💠	21 💠
Power (Watts) @ 25 C	Same as Same as	1.0		0.40		0.20		0.40				08.0
Status	R A&M	я	ار د	ч _{Ст}	Ь	Ъ	Ъ	Д	~	Ъ	Ъ	Ъ
Package	P-6(2) P-6	P-16	P-3	F-4 P-11A	P-15	P-1	D-65	P-65	P-65	P-65	P-65	P-65
Description	Alloy Ge P-N-P Alloy Ge N-P-N	Alloy Ge P-N-P	Si Planar N-P-N	Diff. Ge P-N-P	Alloy Ge P-N-P	Si Planar N-P-N	Si Planar N-P-N	S_{i}	Si Planar N-P-N	Si Planar N-P-N	Si Planar N-P-N	45F†† Si Planar N-P-N
Code	35B 36A	37A	40A††	42A**	43A	44A††	45A††	45B††	45C††	45D†† S	45E††	45F††

Note: Power ratings are for free air operation. All electrical values are "Initial Limits" $\triangle t_S = 15 \text{ nsec}$ †† Epitaxial R = Restricted (Check use with Applications Engineer) $^+*8\mathrm{VCEO}$ ** $^+*4\mathrm{s}$ $^-\star$ hfe $^+$: $^+$ G $^-$ C $^$ P = Preferred

4 Dual transistor (two wafers in same enclosure) each exhibiting the electrical characteristics given.

This is particularly Care should be taken if any of the breakdown characteristics such as BVCEO, BVCES, BVCER are exceeded. true of epitaxial transistors which have low collector body resistance.

TRANSISTORS

(Med) (Min) ♦ (Mc)	•	•	_	_	_		
$_{ m T^{ m f}}^{ m T}$	006	200	650	920	009	95	
t _s + t _f (nsec) (Max.)							_
td + tr (nsec) (Max.)							
-hfb -hFB (Min.)	1100-300	†75-150	†30-200	†50-100	135-75	†40-250	
V _{CE} (sus) BV _{CEV} ♦ (Min)	15	30	35	35	30	35	
BVEBO (Min.)	4.0	4.0	4.0	4.0	4.0	5.0	
ICBO (µAdc) (Max.)	0.08	1.0	1.0	1.0	1.0	0.01	
BVCBO BVCES (Min.)	21 ♦	35	35	35	35	20	
Power (Watts) @ 25 C	1.0	4.0	4.0	4.0	4.0	0.36	
Status	R	д	Ъ	æ	R	Д	
Package	P-65	P-64	P-64	P-64	P-64	P-1	
Description	Si Planar N-P-N	Si Planar N-P-N	Si Planar N-P-N	Si Planar N-P-N	Si Planar N-P-N	Si Planar P-N-P	
Code	***45G††	46A††	46C++	F-56578 46D††	1		2686911
	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Package Status © 25 C (Min.) Pc65 R 1.0 21ϕ 0.08 4.0 15 Process -hfb 100-300	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	Description Package Status Sta	Description Package Status Power BVCBO ICBO BVCEV PhFB PhFB	Description Package Status © 25 C (Min.) (Min.)	Description Package Status BVCBO ICBO BVEBO BVCEV Hin.) Watts BVCES Hin.) Hin. H

All electrical values are "Initial Limits" $\triangle t_S = 15 \text{ nsec}$ Note: Power ratings are for free air operation. P = Preferred

Care should be taken if any of the breakdown characteristics such as BVCEO, BVCES, BVCER are exceeded. This is particularly true of epitaxial transistors which have low collector body resistance.

P-N-P-N DEVICES

					1				
Code	Description	Package Status	Status	I (Amps)	BV _F (Min.)*	BVR (Min.)	I _B for BV _F (mAdc) (Max.)	IH (mAdc) (Max.)	trr (nsec) (Max.)
27A 27B 27C(F-56522) 27D(F-56595) 34A 443A	3-Term PNPN Si 3-Term PNPN Si 3-Term PNPN Si 3-Term PNPN Si 3-Term PNPN Si 2 Term PNPN Si	P-2 P-2 P-2 P-2 P-70	라 # # # 라 라	0.10 0.10 0.10 0.10 5.0	200 350 200 200 100	200 350 200 200 100	0.4 10 1.0 10 0.165 10 .0575 10	*10.0 *10.0 * 3.0 **10.0 **7.0	00

P = Preferred R = Restricted (Check use with Applications Engineer) All Electrical values are Limits Throughout Life.

* For 3 Terminal Devices with RBE = 1000 ohms ** For 3 Terminal Devices with RBE = 0 ohms

							-						
				Power	ir (surge)	if (surge)	To (Ade)	BV @	IR	VF @	IF (Adc)	Is @	VR (Vdc)
Code	Description	Package	Status	@ 25 C	(Max.)	(Max.)	(Max.)		(harran)	(Max.)	(Min.)	(Max.)	(1)
420B	Si Alloy	P-32B	A&M	0.40			.225	200	200	2.0	.010	0.1	160
420D	Si Alloy	P-32B	A&M	0.40			.375	39	200	1.0	.020	0.1	32
420G	Si Alloy	P-32B	A&M	0.40			300	120	200	2.0	.100	0.1	100
425A	Si Diff	P-31A	ፊ	*10.0		100	10.0	250	10	1,15	10.0	0.6	200
425L	Si Diff	P-31A	Ъ	*10.0		20	7.0	200	10	1,45	7.0	5.0	160
** 425AB	Si Diff	P-31B	Ъ	*10.0		100	10.0	250	10	1,15	10.0	3,0	200
426A	Si Diff	P-30B	4	1.0	3.0	30	1.0	250	10	1.1	1.0	1.0	200
426F	Si Diff	P-30B	д	1.0	4.0	20	1.0	200	10	1.05	1.0	1.0	400
426G	Si Diff	P-30B	В		2.0	12	009	1200	25	2,1	09.0	3.0	1000
426H	Si Diff	P-30B	24		1.5	8.0	.400	1800	25	3.0	0.40	3.0	1500
426J	Si Diff	P-30B	댐		1.0	6.0	.300	2400	25	3.7	0.30	3.0	2000
426K	Si Diff	P-30B	Д		4.0	20	1.0	009	10	1.05	1.0	1.0	200
426L	Si Diff	P-30B	Д	1.0	12.5	12	009	800	10	2.1	09.0	3.0	650
426AF	Si Diff	P-30B	ж	1.0		20	1.0	290	10	1,05	1.0	.065	200
435D	Si Diff.	P-29	A&M	0.25		12		120	10	06.0	0.25	0.10	100
440A	Si Diff	P-32B	В	0.75		12	. 750	1001	1.0	1,15	0.75	1.0	100
440B	Si Diff	P-32B	æ	09.0			009.	250	200	1.1	**0.60	0.1	200
446F	Si Diff	P-34A	<u>م</u>	0.40		3.0	.400	400-920	10	1.0	0.40	2.0	320
446K	Si Diff	P-34A	Ъ	0.40		3.0	.400	600-950	10	1.0	0.40	2.0	480
458A	Si Diff	P-39	Ъ	01.0			.100	75	5.0	1.1	0.40	0.20	40
460A	Si Diff††	P-18	д	09.0			.250	***002		1.2	0.250	1.0***	160
460B	Si Diff†	P-18	20€6 *	09.0		2.0*	.400	7.5		1.1	.400	0.20	09
461A	Si Diff††	P-59	Д	0.75			. 750	200		1.2	0.250	1, 0***	160
485A	Si Diff	P-72A	10/65*	*10.0		100	10.0	250		1,15	10.0	3.0	200

RECTIFIERS

4 Diodes in Bridge Configuration Anticipated availability from WECO Reverse polarity; case is positive for reverse bias P = Preferred
R = Restricted (Check use with Applications Engineer) ** Maximum
Note: Power ratings are for free air operation *** Between adjacent terminals
ABOVE QUICK SELECTION DATA NOT TO BE USED FOR CIRCUIT DESIGN USE OFFICIAL DATA SHEET

10 WATT VOLTAGE REGULATORS

TCBV (%/°C) (Nom.)	880 80 70 02	80 80 50 85	80 70 60 85	50 00 00
	. 080 . 080 . 080 . 070	.080 .080 .050 .050	.080 .070 .060	.050
@ IR) (mAdc)	30 50 50 50 10	20 200 200 50	100 100 50 50	200 18 18
bz (ohms) (Max.)	12 4.0 2.0 2.0 20	12 12 3.0 8.0 8.0	5.0 3.0 8.0	3.0 100 100
VR (Vdc)	14.5 9.5 9.5 5.0	17.5 17.5 6.5 21.5 21.5	14.4 12 9.5 20	6.5 115 115
IS © (µAdc) (Max.)	3.0 3.0 1.0 1.0	1.0 3.0 10 4.0 50	4.0 4.0 3.0 3.0	10 3.0 3.0
@ IF (Adc) (Min.)	10 10 10 10	10 10 10 10	10 10 10 10	10 10 10
V _F (Vdc) (Max.)	1.25 1.25 1.25 1.25	1.25 1.25 1.25 1.25 1.25	1,25 1,25 1,25 1,25	1.25 1.25 1.25
IR (mAdc)	30 50 50 50 10	20 20 200 50 50	100 100 1.0	200 18 18
BV @ (Vdc)	22 ± 3, 5% 18 ± 10% 12 ± 10% 15 ± 10% 8, 65 ± 5%	22 ± 10% 22 ± 5% 8.2 ± 5% 27 ± 5% 27 ± 5%	$18 \pm 5\%$ $15 \pm 5\%$ $12.4 \pm 2\%$ $24 \pm 5\%$	$8.2 \pm 5\%$ $140 \pm 5\%$ $140 \pm 5\%$
Status	民民中民中	다다다다대	ж г ч ч	A H H
Package	P-31A P-31A P-31A P-31A P-31A	P-31B P-31A P-31A P-31A P-31B	P-31B P-31A P-31A P-31A	P-31B P-72A P-72B
Description	Si Diff. Si Diff. Si Diff. Si Diff. Si Diff.	Si Diff. Si Diff. Si Diff. Si Diff. Si Diff.	Si Diff. Si Diff. Si Diff. Si Diff.	Si Diff. Si Diff. Si Diff.
Code	425C 425D 425E 425F 425G*	425H** 425J 425M 425N 425P**	425R** 425T 425U† 425AA	425AC** 485W 485Y**

* Intended for low temperature coefficient voltage regulator applications-1 Watt.

 $P=Preferred \\ R=Restricted (Check use with Applications Engineer) \\ ABOVE QUICK SELECTION DATA NOT TO BE USED FOR CIRCUIT DESIGN - USE OFFICIAL DATA SHEET.$

^{**} Reverse polarity; case is positive for reverse bias.

1.0 WATT VOLTAGE REGULATORS

	TCBV (%/°C) (Nom.)	080 080 080 080 080	.090 .005 .05 .003	.085 .090 .070 .070	.030
	(mAdc) ((20 10 20 10	20 10 20 10	5.0 2.0 10 10	2.0 50
	bz (ohms) (Max.)	30 30 10 25 20	5.0 15 20 8.0 20	50 175 17 75 30	350 7.0
	VR (Vdc)	55 18 9.5 14.5	5.0 14.5 5.0 6.0	21.5 60 12 26.0 17.5	85.0 3.0
	IS @ (µAdc) (Max.)	3.0 1.0 5.0 1.0	30 3.0 50 1.0 50	2.0 2.0 2.0 2.0	2.0 400
	IF (Adc) (Min.)	1.0	1.0	1.0 1.0 1.0	1.0
	VF @ (Vdc) (Max.)	1.0	1.0	1.0 1.0 1.0	1.0
211101	IR (mAdc)	20 10 20 10	20 10 10 20 10	5.0 5.0 10 10	2.0 50
	BV @ (Vdc)	68 ± 10% 22 ± 10% 12 ± 10% 18 ± 10% 15 ± 10%	8.2 \pm 10% 18 \pm 10% 8.65 \pm 5% 6.8 \pm 10% 8.65 \pm 5%	27 ± 5% 75 ± 5% 15 ± 5% 33 ± 5% 22 ± 5%	105 ± 5% 4.7 ± 5%
	Status	æ c c c c	다저다저氏	4444	R P
	Package	P-30B P-30B P-30B P-30B P-30B	P-30B P-30B P-30B P-30B P-30B	P-30B P-30B P-30B P-30B P-30B	P-30B P-30A
	Description	Si Diff. Si Diff. Si Diff. Si Diff.	Si Diff. Si Diff. Si Diff. Si Diff. Si Diff.	Si Diff. Si Diff. Si Diff. Si Diff. Si Diff.	Si Diff. Si Alloy
	Code	426E† 426M 426P 426R 426R 426S	426T 426U†† 426W 426Y††† 426AB	426AG 426AH 426AJ 426AK 426AK	426AM 470A*

P = Preferred * Reverse polarity; case is positive for reverse bias \dagger 6 amp, surge protector R = Restricted (Check use with Applications Engineer) \dagger 22 amp, surge protector \dagger 6 amp, surge protector ABOVE QUICK SELECTION DATA NOT TO BE USED FOR CIRCUIT DESIGN - USE OFFICIAL DATA SHEET.

0.4 WATT VOLTAGE REGULATORS

-	-															
1	(%/°C) (Nom.)	.040	060.	060.	080.	090*	060.	080.	060.	090•	090	.035	090.	.065	.085	060.
@ I _R	s) (mAdc)	15.0	10.0 0.75	0.75	2.5	0.75	10	10	10	0.75	10	10	10	10	5.0	5.0
) zq	(ohms)	6.5	160	400	200	27	100	100	100	27	09	0. 9	7.0	10	26	35
@ V _R	(Vdc)	3.0	10 40	85	16	4.0	10	8.0	10	4.0	0 . 9	4.5	6.5	9,5	14.5	21.5
I _S	(µAdc) (Max.)	5.0	0.1 0.1	0.1	0.1	1.0	0.1	0.1	0.1	1,0	0.1	200	2.0	1.0	1.0	1.0
ı IF	(Adc) (Min.)	. 030	.100	0.10	0.20	0.10	0.02	0,02	0.02	0.10	0.02	0.40	0.40	0.40	0.40	0.40
V _F	(Vdc) (Max.)	1.0	2.0 2.0	2.0	2.0	1.5	1.0	1.0	1.0	1.5	1.0	1.0	1.0	1.0	1.0	1.0
I.B.	(mAdc)	10.0	0.50	0.50	0.50	0.50	0.50	0.50	1.0	0.5	0.5	10.0	10.0	10.0	5.0	5.0
BV @	(Vdc)	6 ± 10%	17.5 ± 14% 59 ± 12%	$118 \pm 8\%$	$22.5 \pm 10\%$	8.2 ± 10%	$15 \pm 10\%$	$12 \pm 10\%$	$18 \pm 5\%$	$8.2 \pm 5\%$	$10 \pm 10\%$	$6.2 \pm 5\%$	$8.2 \pm 10\%$	$12 \pm 10\%$	$18 \pm 5\%$	$27 \pm 5\%$
	Status	A&M	A&M A&M	A&M	A&M	A&M	A&M	A&M	A&M	A&M	A&M	Д	Д	Д	Ъ	Ь
	Package	P-32B	P-32B P-32B	P-32B	P-32B	P-32B	P-32B	P-32B	P-32B	P-32B	P-32B	P-34A	P-34A	P-34A	P-34A	P-34A
	Description	Si Alloy	Si Alloy Si Alloy	Si Alloy	Si Alloy	Si Alloy	Si Alloy	Si Alloy	Si Alloy	Si Alloy	Si Alloy	Si Diff	Si Diff	Si Diff	Si Diff	Si Diff
	Code	420A	420E 420H	420J	420K	420M	420N	420P	420R	420S	420T	446B	446C	446D	446E	446G

*Anticipated availability from WECO.

R = Restricted (Check use with Applications Engineer)

P = Preferred

0.4 WATT VOLTAGE REGULATORS

[
Tra Ott	(%/°C) (Nom.)	. 105 . 070 . 075 . 090	. 090 . 065 . 090 . 090	.065 .020 .020
I.	K (mAdc)	2.0 5.0 5.0	1.0 1.0 1.0 1.0	10 20 20 10
bz @	(ohms)	210 9.0 24 30	350 7.0 285 345 8.0	10 18 18 7.0
@ V.	K (Vdc)	37.5 8.0 12 17.5	80 6.5 49.5 72.5	9.5 3.0 6.5
ľ	Б (µAdc) (Мах.)	1.000.1	2.000.000.000.000.000.000.000.000.000.0	1.0 250 250 2.0
I I	r (Adc) (Min.)	0.40 0.40 0.40 0.40	0.40 0.40 0.40 0.40 0.40	0.40 0.20 0.20 0.20
N TA	(Vdc) (Max.)	00000	00000	1.0 1.0 1.0
I	R (mAdc)	2.0 10.0 5.0 5.0	1.0 10.0 1.0 1.0 10.0	10.0 20.0 20.0 10.0
BV @ I, V, @ I,	(Vdc)	47 ± 5% 10 ± 5% 15 ± 5% 22 ± 5% 30 + 5%	44444	12 ± 5% 4.7 ± 10% 4.3 ± 5% 8.2 ± 5%
	Status	4	4444	P P 2Q66★ 3Q66★
	Package	P-34A P-34A P-34A P-34A P-34A	P-34A P-34A P-34A P-34A P-34A	P-34A P-34A P-34A P-39
	Description	Si Diff Si Diff Si Diff Si Diff	Si Diff Si Diff Si Diff Si Diff Si Diff	Si Diff Si Alloy Si Alloy Si Diff
	Code	446H 446L 446M 446N 446N	446T 446U 446W 446W 446Y	446AD 448A 448B 459E

* Anticipated availability from WECO.

R = Restricted (Check use with Applications Engineer)

P = Preferred

ABOVE QUICK SELECTION DATA NOT TO BE USED FOR CIRCUIT DESIGN - USE OFFICIAL DATA SHEET.

SWITCHING DIODES

		Power	9	Ĺ	VF	@ IF	© SI	@ V _R	C	trr @	$I_{F} = I_{R}$
Package	Status	(Watts) @ 25 C	BV (Min.)	⁴ R (µAdc)	(Vdc) (Max.)	(Adc) (Min.)		(Vdc)	(pf) (Max.)	(max.)	(mAdc)
	A &M	09.0	80	500	1.1	0.02	10	50.0	100	0.50	10
	Ь	*5.0	100	10	1.3	2.0	3.0	80	800	0.20	30
	Ъ	*10.0	200	10	1.45	7.0	5.0	160	400	0.20	100
	Ъ	*10.0	250	10	1.15	10.0	3.0	200		3, 5-5, 5	1500
	Ъ	1.0	800	10	2.1	09.0	3.0	650	20	0.1	10
	P	1.0	120	10	**1.35	**1.35	1.0	20	45	0.10	100
	Ь	1.0	120	10	1.0	1.0	1.0	100	100	0.20	100
	A&M	0.10	40	5.0	1.0	0.01	0.015	20	4.0	0.004	10
	A&M	0.25	40	5.0	1.0	0.01	0.015	20	3.5	0.004	10
7	4&M	0.25	40	5.0	0.72	0.002	0.015	20	4.0	0.004	10
	Ъ	0.40	120	5.0	1,1	0.40	2.0	100	25	0.05	100
	A&M	0.10	40	5.0	1.0	0.01	0.025	20	3, 5	0.004	10
	Ъ	0.40			2.30	0.0025	2.0	150	15	0.04(Min)	

 \dagger @ $\rm V_{R}$ = 0 Vdc except 449A @ $\rm V_{F}$ = 1.0 Vdc. & 420L @ $\rm V_{R}$ = 4.5 Vdc

†† Level Shifter: V_F = 1.53 Vdc Min. @ 70 μ Adc. Stored Charge=400 pCb @ i_f =2 mAdc, i_r =10 mAdc.

⊕ Epitaxial

P = Preferred

R = Restricted (Check use with Applications Engineer)

NOTE: Power ratings are for free air operation.

*** Switched Power ** Peak Pulse

* With Heat Sink

SWITCHING DIODES

wer by by control by c	Power (Watts) (@ 25 C (0.10*** 0.10*** 0.10*** 0.10***	* * * *	Power (Watts) (Watts) (Status @ 25 C (P 0.10*** P 0.10*** P 0.10*** P 0.10***
0	0.10	Ъ	Si Diff. P-39 P
0	3 0.10	R	Si Diff. P-39 R

† @ $\rm V_R$ = 0 Vdc except 449A @ V $_F$ = 1.0 Vdc. & 420L @ V $_R$ = 4.5 Vdc

R = Restricted (Check use with Applications Engineer)

P = Preferred

NOTE: Power ratings are for free air operation.

Epitaxial

†† Level Shifter: $V_F=1.53$ Vdc Min. @ 70 μ Adc. Stored Charge=400 pCb @ $i_f=2$ mAdc, $i_r=10$ mAdc.

* With Heat Sink ** Peak Pulse

GERMANIUM DIODES

Code	Description	Package	Status	Power (Watts)	BV (Vdc) (Min.)	I _R (mAdc)	$egin{array}{c} \Gamma_{\mathbf{R}} & @ \ (\mu\mathrm{Adc}) \ & (\mathrm{Max.}) \end{array} ight $	$\stackrel{@}{=} \stackrel{V_{\mathbf{R}}}{\text{(Vdc)}}$
A		P-43	Ъ	0.20	09		20/820	2/50
ET F		P-43	<u>ط</u> د	0.20	140		500	50 5/50
400F	Ft. Ct.	F-43 P-43	ਮੁਟ	0.20	09		1000	50
Н		P-43	8	0.20	09		20/850	5/50
J		P-43	Ъ	0.20	140		20/850	5/50
A	Pt. Ct.	P-32B	R	0.20			3, 5/35	5/25
Α		P-40	Д	Same as	400A ex	except axia	axial leads	
Ħ		P-40	Ь	Same as	400F ex	400F except axial leads	l leads	
441H		P-40	씸	Same as	400H ex	400H except axial leads	l leads	
ь		P-40	R	Same as	400J ex	400J except axial leads	l leads	

P = Preferred

R = Restricted (Check use with Applications Engineer)

Note: Power ratings are for free air operation

MICROWAVE DIODES

								IS		၁	
			Power	BV @	IR	$ m V_F$ @	Ţ	IR ♦ @	y VR	◆ LO	
			(Watts)	(Vdc)	(mAdc)	(Vdc)	(Adc)	(hAdc) (Vdc)	(Vdc)	(bt)	
Code	Package	Status	@ 25 C	(Min.)		(Max.)	(Min.)	(Max.)		(Max.)	Major Application
404		A & TM	04.0	~3.0		1.0	. 020	150	1.0		High Level Mixer
404		A 8-1/1	07.0	2				500	9.0		High Level Mixer
404D		TAT OF TAT	2.		_	,			,		High I one I Misses
404C		A&M	0.40	~3.0		1.0	.040	000	T: 0		nign Level Mixer
404D		A&M	0.40	~3.0		1.0	.040	200	1.0		High Level Mixer
405B		ĸ	0.40	^3.0							Detector
405C		Я	0.02	~3.0							Detector
405D		A&M	0.40	~3.0							Detector
405E ††		R	0.30					100	1.0		Detector-Monitor
406A		Ж	0.02	~3.0				•			Converter
406B	P-26	В	0.02	~1.0		0.2	.0004	40 +	0.2		Converter
431A	P-25B	A&M	0.50	~25		.80	.10	100	7.5		Limiter
444A	P-27	A & M	0.20					100	2.0		Limiter
445A	P-44	A&M	0.15			0.55	0.01	1,0	1.5	1.7	Converter
_				_							

P = Preferred
R = Restricted (Check use with Applications Engineer)
Note: Power ratings are for free air operation.
ABOVE QUICK SELECTION DATA NOT TO BE USED FOR CIRCUIT DESIGN - USE OFFICIAL DATA SHEET

* Matched Pair – Unmounted ** Heat Sink at 25 C *** This rating applies to the pair † Applies for each diode of the pair †† Special vswr requirements

MICROWAVE DIODES

Code	Package	Status	Power (Watts) @ 25 C	BV @ (Vdc) (Min.)	IR (mAdc)	V _F @ (Vdc)	IF (Adc)	IS IR ♦ @ (µAdc) (Max.)	VR (Vdc)	C CT ♦ (pt)	Maior Application
471A*	D-93	<u></u>	***	+15	0 01	-	100	- 0	5	+0 8−1 9	Transmitter Modulator
472B	P-22	: 24	0.05	30	0.01	11	.100	0.0	24	0.6-0.9	Harmonic Generator
72C	P-22	R	0.02	20	0.01	1.2	100	0.1	16	.405485	Parametric Amplifier
72D	P-22	Я	0.02	20	0.01	1.2	.100	0.1	16	.455535	Parametric Amplifier
72E	P-22	ж	0.02	20	0.01	1.2	.100	0.1	16	. 505 585 ♦	Parametric Amplifier
72F	P-22	R	0.02	20	0.01	1.2	.100	0.1	16	. 555-, 635	Parametric Amplifier
473A	P-21	Я	2.0**	09	0.01	1.1	100	1.0		3.0-6.0	Harmonic Generator r
73B	P-21	24	3.0**	- 08	0.01	1.0	.100	1.0		11-19	Harmonic Generator r
73C	P-21	я	4.0**	7.0	0.01	1.0	100	1.0	09	46-68	Harmonic Generator r
80A	P-38	R	0.03	15	0.01	1.1	.100	0.1		0.3-0.6	70 Mc Gates
488A	P-38	R	0.05	3.0				200	1.0		I. F. Detector

P = Preferred

R = Restricted (Check use with Applications Engineer)
Note: Power ratings are for free air operation.
ABOVE QUICK SELECTION DATA NOT TO BE USED FOR CIRCUIT DESIGN - USE OFFICIAL DATA SHEET

*** This rating applies to the pair † Applies for each diode of the pair †† Special vswr requirements * Matched Pair - Unmounted ** Heat Sink at 25 C

MULTIPLE DIODES

appropriate Applications Engineer. ABOVE QUICK SELECTION DATA NOT TO BE USED FOR CIRCUIT DESIGN - USE OFFICIAL DATA SHEET. These diodes have been designed for specific applications. For further information contact the P = PreferredR = Restricted (Check use with Applications Engineer)

MULTIPLE DIODES

Code	Package	Status	Description
409A	P-74	A&M	Two 404 Types with two leads welded together Ten 400 Types mounted on a plate with mounting brackets Two 400 Types mounted on a plate with mounting bracket Twelve 405B's mounted between plates with a mounting bracket
410A	P-61	R	
411A	P-54	R	
413A	P-75	A&M	
414A	P-76	A&M	Four 405B's mounted between plates with a mounting bracket Four 405B's mounted on a plate and covered by a metal can Two 405's with overall NF = 10 db max. Replace with 420G Four 405B's mounted between plates
415A	P-77	A&M	
416C	P-25A	R	
417B	P-79	A&M	
418A	P-78	A&M	
421A	P-48	R	Two 420 Types mounted on a plate
421C	P-48		Two 420 Types mounted on a plate
421D	P-48	яв	Two 420 Types mounted on a plate
421E	P-48		Two 420 Types mounted on a plate
422B	P-50		Four 420 Types mounted on a plate
426N	P-30C	R	A 68V 10% Regulator and 200V Rectifier back-to-back
427A	P-25B	A&M	Two 431A's
433A	P-49	A&M	Two 420 Types in series mounted on a plate

applications. For further information contact the These diodes have been designed for specific appropriate Applications Engineer. R= Restricted (Check use with Applications Engineer) applic ABOVE QUICK SELECTION DATA NOT TO BE appro USED FOR CIRCUIT DESIGN - USE OFFICIAL DATA SHEET. P = Preferred

MULTIPLE DIODES

Code	Package	Status	Description
433B 434B 437A 438A	P-49 P-47(2) P-42 P-46(2)	A&M A&M A&M R	Two 420 Types in series mounted on a plate Four si. diff. diodes matched for forward impedance Seven 432 Types (unmounted) Matched for VF at 20 µAdc, 200 µAdc, and 2 mAdc @ 120 C
439A 442A 462A 463A 464A	P-45(2) P-35 P-11B P-55 P-56	R P R	Matched for V _F at 20 μAdc, 200 μAdc, and 2 mAdc @ 120 C Four 432 Types Ge. full-wave bridge in single encapsulation Four 426J's in series – molded Four 426G's in full-wave bridge – molded
464B 464C 465A 465B 466A	P-56 P-56 P-39 P-39 P-53	አ ਯ ਯ ਯ ਯ ਯ ਯ ਯ ਯ ਯ ਯ ਯ ਯ ਯ	Four 426J's in full-wave bridge – molded Four 426 Type diodes in full-wave bridge – molded Seven 458A's matched – unmounted Seven 458C's matched – unmounted Four 458A's mounted on board
475A 477A 478A 478B 482A	P-11C P-31 P-57 P-57 P-63	яяя	Matched pair of diode elements in a single encapsulation Four 425S's matched for +10% t _{rr} - unmounted Five 426L's connected in series - molded Four 426G's connected in series - molded Eight diode elements with common cathodes in single encapsulation

applications. For further information contact the These diodes have been designed for specific P = Preferred
R = Restricted (Check use with Applications Engineer) applications. For further informat ABOVE QUICK SELECTION DATA NOT TO BE appropriate Applications Engineer. USED FOR CIRCUIT DESIGN - USE OFFICIAL DATA SHEET.

MULTIPLE DIODES

Code	Package	Status	Description
482B	P-63	Д	Eight diode elements with common anodes in single encapsulation
483A	P-39	Ъ	Four 458C's matched - unmounted
484A	P-62	В	Two mounted diodes, each in a TO-18 package, matched for forward
			impedance
484B	P-62	R	Same as 484A, except different forward impedance match
487A	P-68	Ч	Four 446 Type diodes in bridge configuration - molded
487B	P-68	Д	Same as 487A with lower pulse handling capability
489A	P-66	Ъ	Two mounted diodes, each in a TO-18 package, matched for forward
			impedance
489B	P-66	C ₄	Same as 489A, except different forward impedance match
491A	P-11B	C ₄	Si full-wave bridge in single encapsulation. Polarity ground

applications. For further information contact the These diodes have been designed for specific USED FOR CIRCUIT DESIGN - USE OFFICIAL DATA SHEET. R = Restricted (Check use with Applications Engineer) ABOVE QUICK SELECTION DATA NOT TO BE P = Preferred

SPECIAL USE DIODES

Code	Package	Status	Description
426AA	P-30B	R	Variable capacitance diode, $C = 900$ pf @ V_R 1.0 Vdc $BV = 13.1 - 13.6$ @ $I_R = 20.0$ mAdc Symmetrical surge protector, \pm 18 volt limiter Variable capacitance diode, $C = 28$ pf @ $V_R = 4$ Vdc Variable capacitance diode, $C = 28$ pf @ $V_R = 4$ Vdc Variable capacitance diode, $C = 28$ pf @ $V_R = 4$ Vdc Variable capacitance diode
426AE	P-30B	2Q66★	
426AN	P-30B	R	
446J	P-34B	R	
446P	P-34B	R	
446AA	P-34B	R	
446AB 446AC 457A 474A 476A to AC	P-34A P-34A P-39 P-12 P-29	出 出 出 出 出	Same as 446F except if (surge) 30 A. for 1 MSec. Same as 446T except 100% life tested for 1000 hours Variable capacitance diode (High Q), C=16 pf @ VR 5.0 Vdc Pin Variolosser Diode in TO-18 type package Same as 446A to AC except electrically insulated body
479A	P-10	ж ж	Silicon ESBAR diode in three leaded package
481A	P-28		One 426J-molded

*Anticipated availability from WECO.

R = Restricted (Check use with Applications Engineer)
ABOVE QUICK SELECTION DATA NOT TO BE USED FOR CIRCUIT DESIGN
USE OFFICIAL DATA SHEET.

P = Preferred

	g	
	TSF (db/°F) (Max.) Major Application	x 10-4 R. F. Detector
	TSF (db/°F) (Max.)	9 x 10 ⁻⁴
	Diff. Sens. (mVdc/db) (db/°F) (Min.)	4.0
	RS (ohms)	.170310 6.5-13.5 4.0
O DIODES	CTv (pf)	.170310
Ge BACKWARD DIODES	Vpvdc)	30-70
Ge I	$ m I_p/I_v$ (Min.)	4.0
	ower Ip (mW) (mAdc) 25 C	.040200 4.0 30-70
	Power (mW) @ 25 C	9.0
	Status	Ж
	Code Package Status	P-23
	Code	486A

P - Preferred R - Restricted (Check use with Applications Engineer)
Note: Power ratings are for free air operation
ABOVE QUICK SELECTION DATA NOT TO BE USED FOR CIRCUIT DESIGN - USE OFFICIAL DATA SHEET.

CERAMIC THIN FILM CIRCUITS

	Delay Time	(Nanosec.)	06	<45	06>	<45	<180	<135	06>	<45	<180	<135	06>	√10	<10	<10 <10	<50	<20	<45	<45	<45	<45	
Noise	Index	DB	-25	-25	-25	-25	-25	-25	-25	-25	-25	-25	-25	-25	-25	-25	-25	-25	-25	-25	-25	-25	-25
		Tolerance	¥3%	±3%	#3%	#3%	#3%	±3%	±3%	#3%	#3%	#3%	#3%	#3%	#3%	±3%	#3%	#3%	#3%	±3%	#3%	#3%	±3%
		Status	ď	വ	Ъ	Ъ	Ъ	Ы	Ъ	Ч	ď	Ъ	<u>d</u>	Д	Ь	Д	H.	ж	Ъ	Д	д	Д	Ъ
		Package	P-85	P-85	P-85**	P-85**	P-84	P-84	P-84	P-84	P-84**	P-84**	P-84**	P-88	P-88	P-88	P-86	P-86	P-85	P-85	P-85	P-87	P-81
		Description and Use*	Two 4-Input Gate	One 4-Input Gate	Two 4-Input Gate - No Power	One 4-Input Gate - No Power	Four 2-Input Gate	Three 2-Input Gate	Two 2-Input Gate	One 2-Input Gate	Four 2-Input Gate - No Power	Three 2-Input Gate - No Power	Two 2-Input Gate - No Power	Emitter Follower	Emitter Follower	Emitter Follower	High Fan Out 4-Input Gate	High Fan Out 2-Input Gate	Two 4-Input IFO Gate	One 4-Input IFO Gate	Two 2-Input IFO Gate	High Fan Out Gate	Time Division Switch
		Code	15A	15B	15C	15D	15E	15F	15G	15H	15J	15K	15L	15M	15N	15P	15R	158	15T	15U	15W	15AA	16A

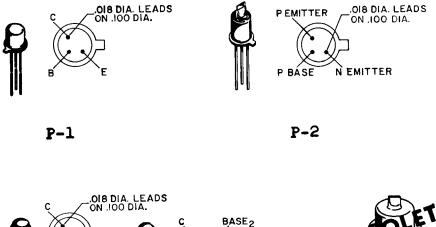
**Refer to package number for electrical schematic.

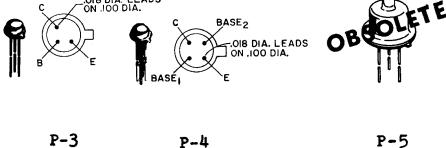
CERAMIC THIN FILM CIRCUITS

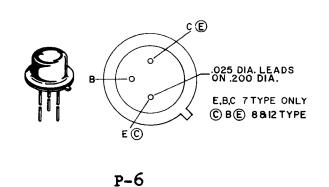
*Refer to package number for electrical schematic.

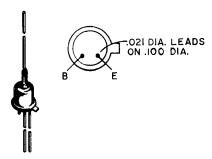
GLASS THIN FILM CIRCUITS

				2	
Code	Description	Package	Status	Tolerance	Use
N	Film (P-82	Ъ	%8∓	
N2	Film	P-82	Д	#3%	
N3	Thin Film Circuit Pack	P-82	Д	78€	TRL Gate
N4	Film	P-82	Ъ	#3%	
SN.	Film Circuit	P-82	Ъ	#3%	
9N	Film Circuit	P-82	Ъ	73%	
N7	Film Circuit	P-82	Ъ	#3%	
8N	Film Circuit	P-82	ф	%£∓	
6N	Film Circuit	P-83	Ъ	78∓	
N10		P-83	Ъ	∓3%	
N11	Thin Film Circuit Pack	P-83	<u>d</u>	#3%	

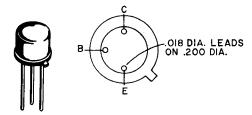




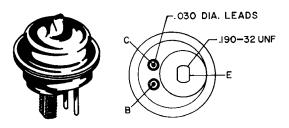




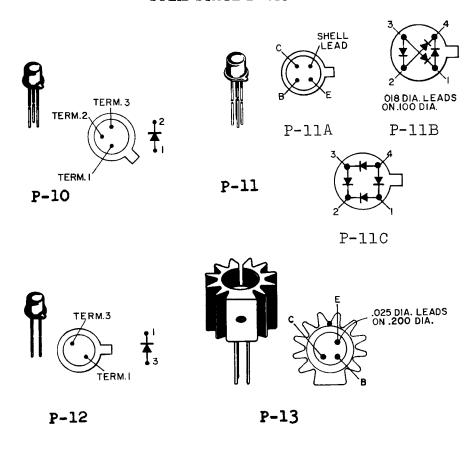
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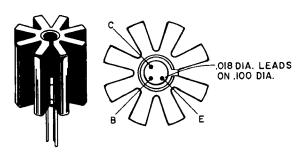


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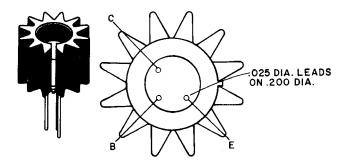


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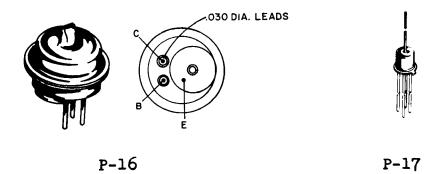


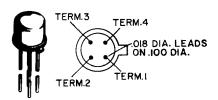


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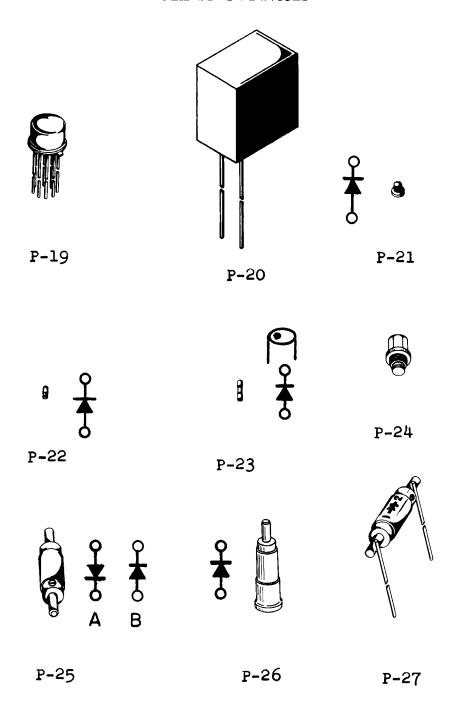


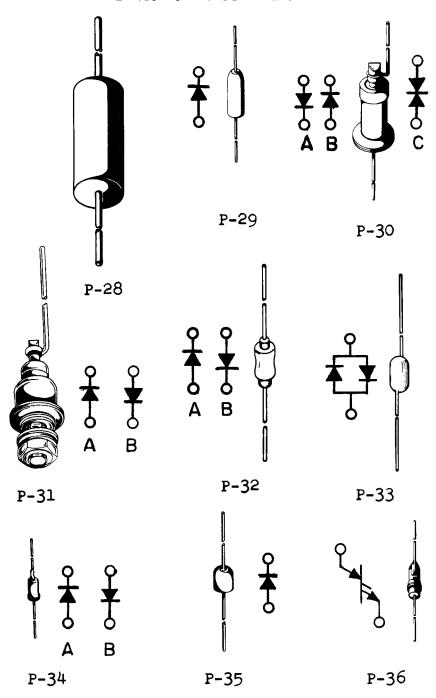
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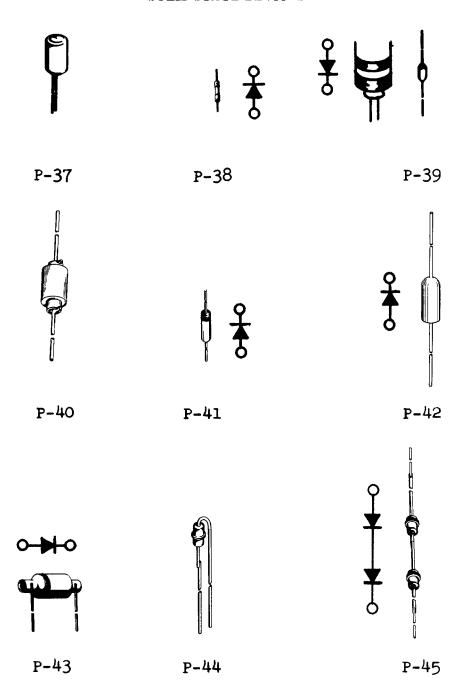


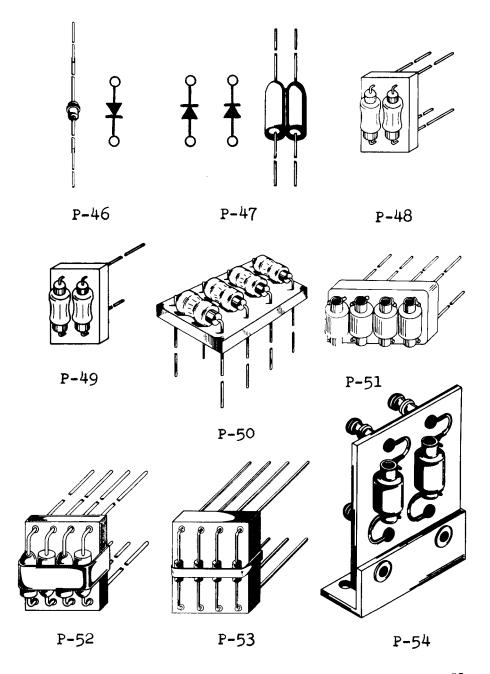


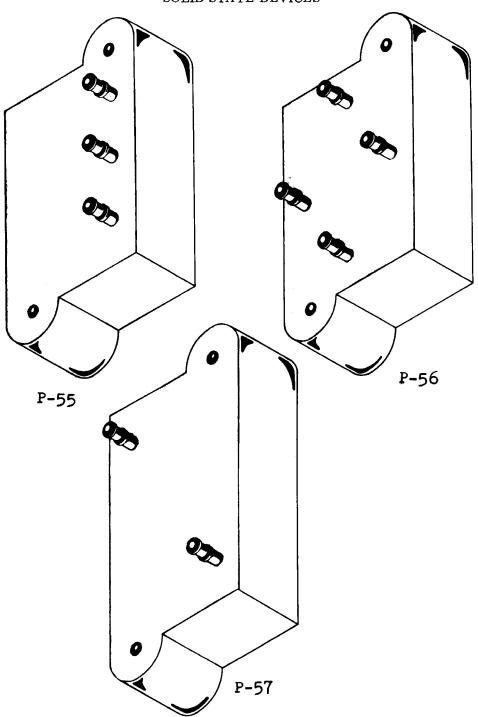
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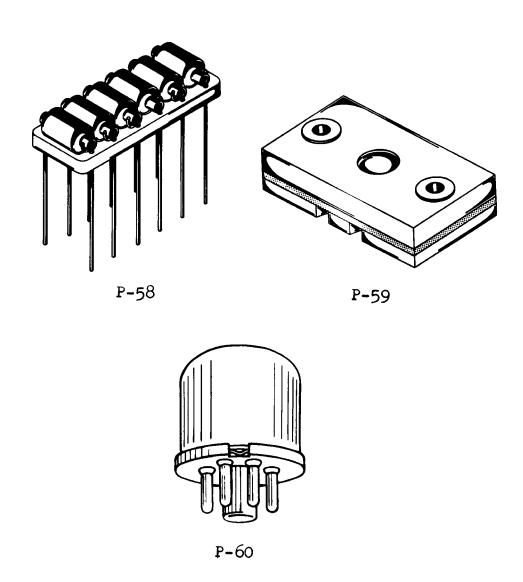


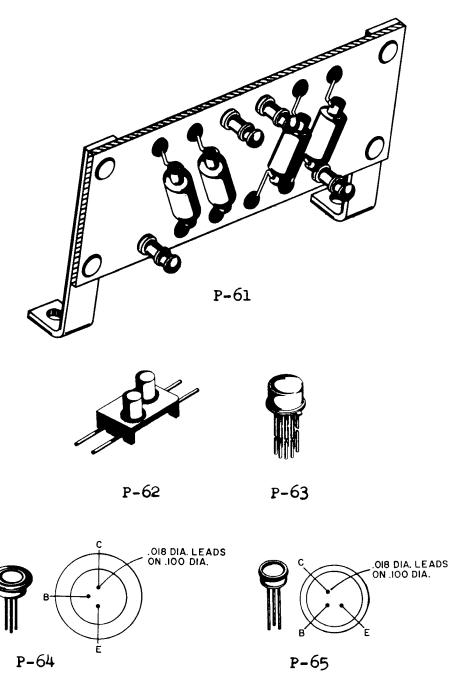


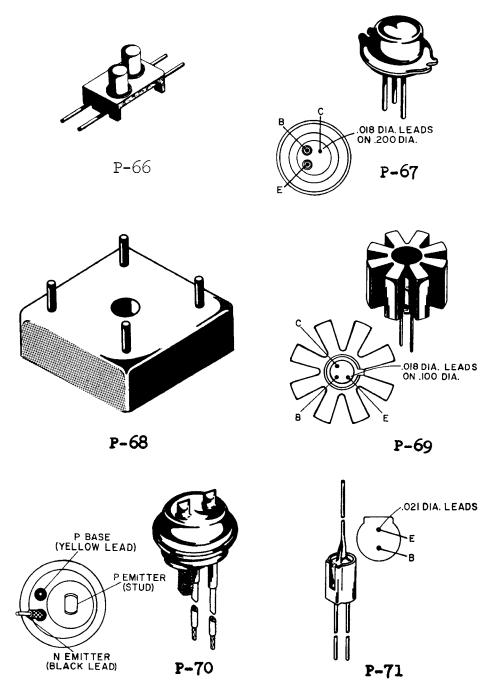


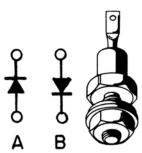


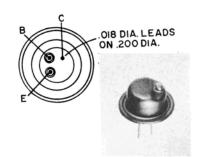




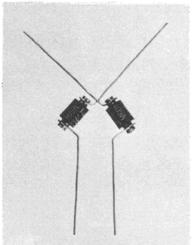






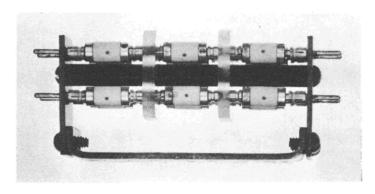


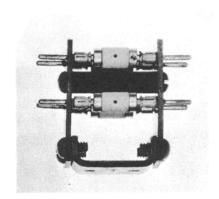
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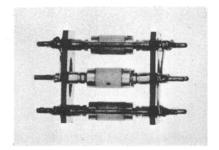
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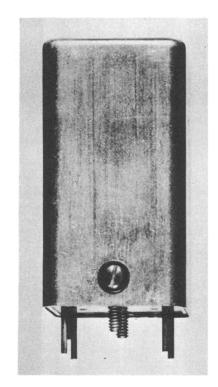




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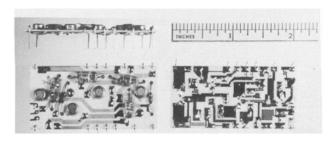
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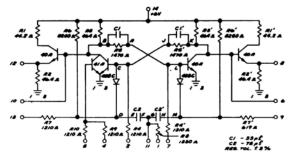


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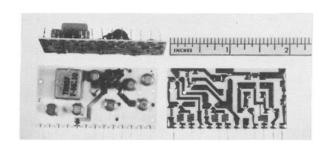


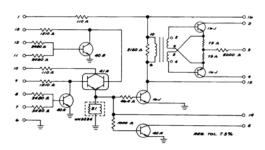
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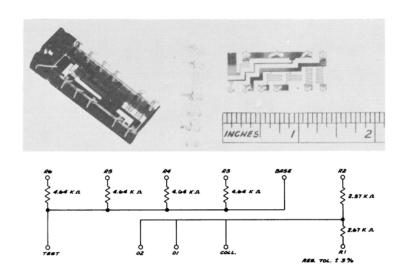


P-80 BINARY COUNTER AND SHIFT REGISTER

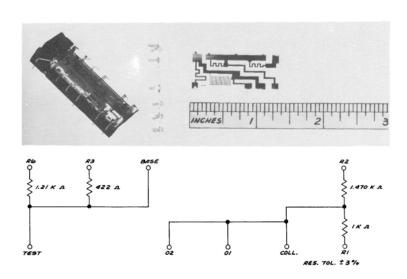




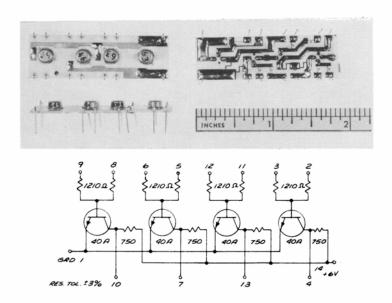
P-81 TIME DIVISION SWITCH



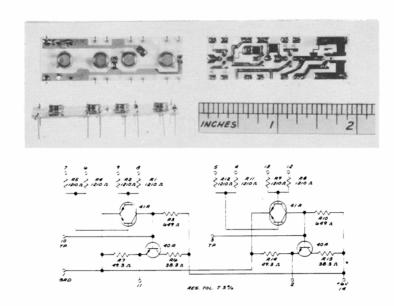
P-82 THIN FILM CIRCUIT PACK



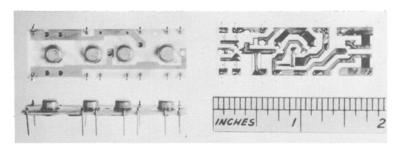
P-83 THIN FILM CIRCUIT PACK

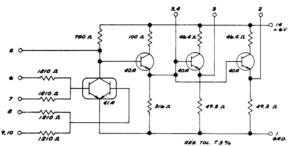


P-84 Four 2-INPUT GATE

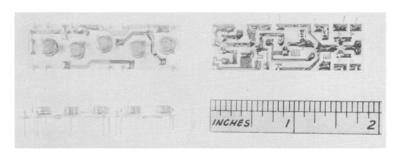


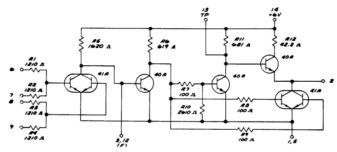
P-85 FOUR 4-INPUT GATE



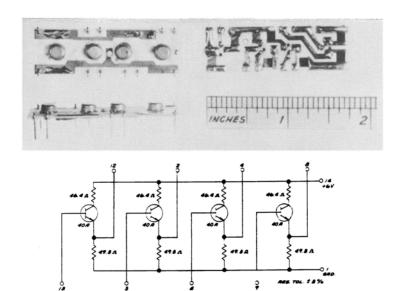


P-86 HIGH FAN-OUT

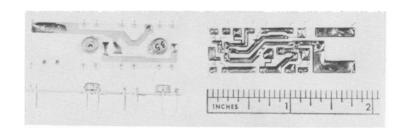


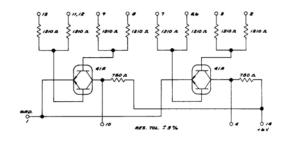


P-87 MODIFIED HIGH FAN-OUT

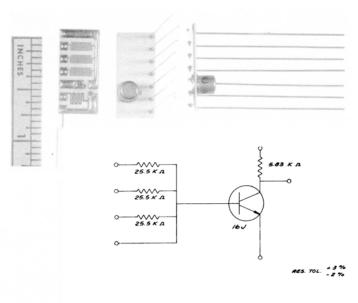


P-88 EMITTER FOLLOWER

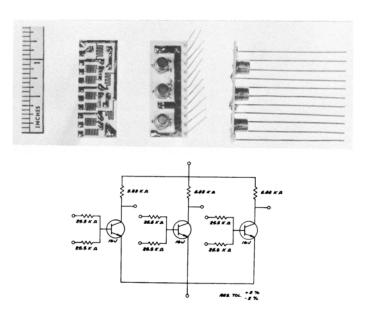




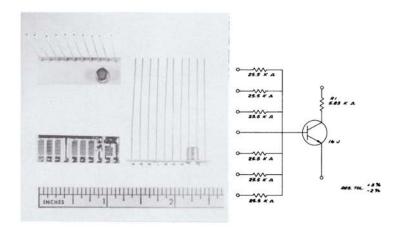
P-89 TWO 4-INPUT GATE



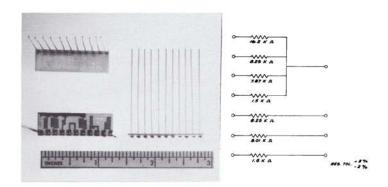
P-90 3-INPUT GATE



P-91 TRIPLE TWO-INPUT GATE



P-92 SIX-INPUT GATE



P-93 LINE CIRCUIT

Appendix A

GLOSSARY OF TERMS

- BV.....Breakdown voltage
 - Breakdown voltage That value of reverse voltage which remains essentially constant over a considerable range of current values.
- BV_{CBO}.....Collector to base breakdown voltage, open emitter.
- ${
 m BV}_{
 m CES}$Collector to emitter breakdown voltage, base dc short circuited to emitter.
- ${\rm BV}_{\rm EBO}$ Emitter to base breakdown voltage, open collector.
- ${\rm BV}_F {\rm Forward~breakdown~voltage~for~PNPN~devices.}$ The maximum forward voltage between ${\rm E_P}$ and ${\rm E_N}$ attained before breakdown under base bias conditions specified.
- ${\rm BV}_R.....{\rm Reverse} \ {\rm breakdown} \ {\rm voltage} \ {\rm for} \ {\rm PNPN} \ {\rm devices.}$ The maximum reverse voltage between ${\rm E}_P$ and ${\rm E}_N$ attained before breakdown is achieved or maximum specified reverse power is reached under base bias conditions specified.
- C_O.....Capacitance of a diode at zero direct current.

 The capacitance at a specified applied ac voltage and frequency and zero direct current.
- fh_{fb}.....Small-signal short-circuit forward-current transfer ratio cutoff frequency.
 - The frequency at which the absolute value of the small-signal short-circuit forward-current transfer ratio is 0.70 times its value at the specified test frequency.

GLOSSARY OF TERMS (Continued)

 f_TExtrapolated unity gain frequency.

The frequency, obtained by extrapolation, at which h_{fe} becomes unity when reduced at a rate of 6db/octave.

h_{fb}.....Small-signal short-circuit forward-current transfer ratio.

Definition - The ratio of the ac output current to the ac input current.

 h_{FR}Static forward-current transfer ratio.

The ratio of the dc output current to the dc input current under the specified test conditions.

h_{fe}.....Small-signal short-circuit forward-current transfer ratio.

The ratio of the ac output current to the ac input current with zero ac output voltage.

ICBO Collector cutoff (saturation) current, open emitter.

The collector cutoff (saturation) current is the dc leakage current in the collector or base terminal when it is reversed biased by a voltage less than the breakdown voltage and with the emitter dc open-circuited.

I Base current, dc.

I F.....Forward current, dc.

 I_{H}Hold current for PNPN devices.

The forward current at which the negative resistance across the device becomes equal to a specified value during the transition from the low impedance to the high impedance state under specified base bias conditions.

Ip.....Reverse current, dc.

APPENDIX A

GLOSSARY OF TERMS (Continued)

Is.....Saturation current.

The dc reverse current which flows through the semiconductor diode under the reverse voltage conditions specified (normally 80% or less of BV).

N_r.....Noise figure.

At a selected input frequency the noise figure is the ratio of the total noise power per unit bandwidth (at the corresponding output frequency) delivered to the output termination, to the portion produced at the input frequency by the thermal noise of the input termination, whose noise temperature is standard (290°K) at all frequencies.

NRTM.....Not ready to manufacture. (Check use with Applications Engineer.)

Power Rating....

That power, which, when applied under specific conditions, yields the junction temperature acceptable for a particular application. In the case of the Quick Selection Guide, the rating for silicon is 125 to 150°C and for germanium is 85 to 100°C with the case at 25°C or ambient as required.

Status....

For convenience, the status is classified into two groups, as follows:

P.....Preferred.

R....Restricted (check use with Applications Engineer).

t_d + t_r.....Pulse delay plus rise time.

The time interval from a point at which the leading edge of the input pulse has risen to a specified part (normally 10%) of its

GLOSSARY OF TERMS (Continued)

maximum amplitude to a point at which the leading edge of the output plus has risen to a specified part (normally 90%) of its maximum amplitude.

t_s.....Pulse storage time.

The time interval from a point at which the trailing edge of the input pulse has decreased a specified part (normally 90%) of its maximum amplitude to a point at which the trailing edge of the output pulse has decreased to the same specified part of its maximum amplitude.

 $t_{g} + t_{f}$Pulse storage plus fall time.

The time interval from a point at which the trailing edge of the input pulse has decreased a specified part (normally 90%) to a point at which the trailing edge of the output pulse has decreased to a specified part (normally 10%) of its maximum amplitude.

t_rr.....Reverse recovery time.

The time between the instant of current reversal from forward to reverse and the instant at which the specified reverse condition is reached.

 $V_{\mathbf{R}\mathbf{F}}$Base to emitter voltage.

 $V_{CE}(sat)$Saturation voltage, collector to emitter.

The dc voltage between the collector and emitter terminals for the specified saturation conditions, (when the transistor output characteristic is essentially a constant voltage).

 ${
m V_{CE}}({
m sus}).....{
m Sustain}$ voltage, collector to emitter.

The voltage which appears between the collector and emitter terminals with specified input current or voltage and output current. (LV $_{\rm CEO}$)

APPENDIX A

GLOSSARY OF TERMS (Continued)

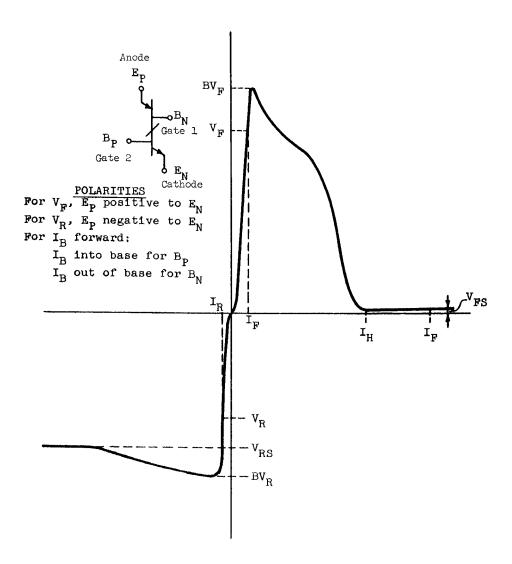
 V_FForward voltage, dc.

V_R.....Reverse voltage, dc.

 V_{RT}Reach through voltage.

That value of reverse voltage for which the depletion layer spreads sufficiently to contact another junction or contact.

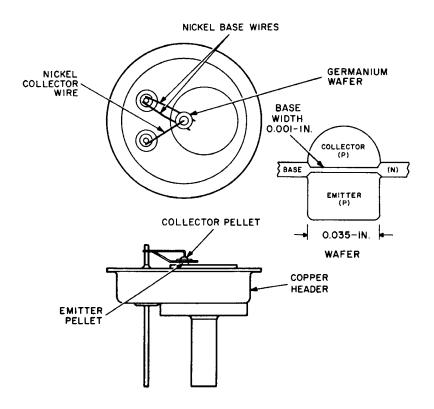
Following is a graphical presentation of symbols for multiple junction devices:



Appendix B

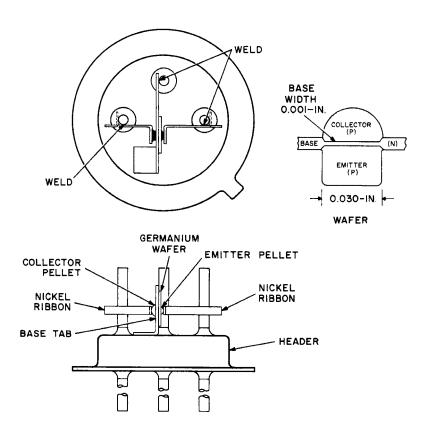
TYPICAL TRANSISTOR AND DIODE CONSTRUCTION

The illustrations on the following pages show the internal construction of some basic transistors and diodes manufactured by the Western Electric Company. Note the minute dimensions of the active regions. Consult the data sheets for electrical ratings. (All dimensions shown on illustrations are approximate.)



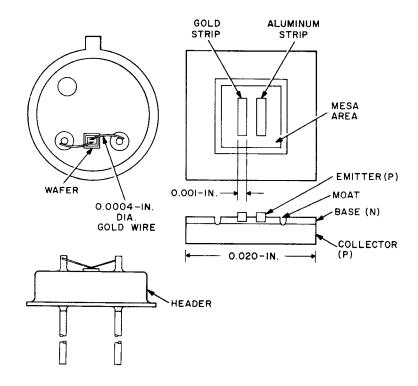
PNP MEDIUM POWER GERMANIUM ALLOY TRANSISTOR - 9 B, D TYPE

The 9 B, D transistor is suitable for use in medium-power, low-distortion amplifier, medium-speed switching and core-driving applications.



MILLIWATT GERMANIUM ALLOY PNP TRANSISTOR - 12 TYPE

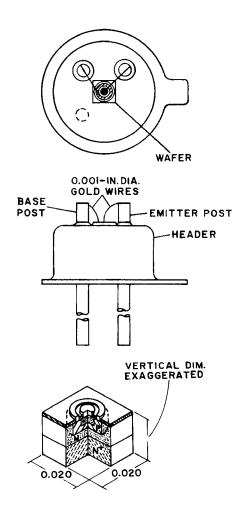
The 12-type transistor is a 1/4-watt, general purpose, PNP germanium alloy junction transistor. It is used principally as a medium-frequency amplifier or medium-speed switch.



MILLIWATT GERMANIUM DIFFUSED BASE (ULTRA-HIGH FREQUENCY) PNP TRANSISTOR - 15 TYPE

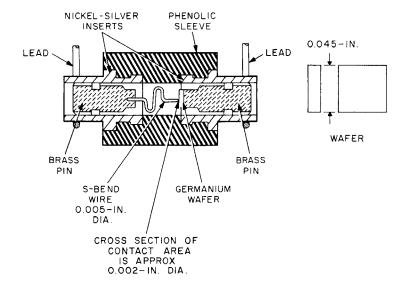
The 15-type transistor is used principally as a VHF amplifier or very fast switch.

APPENDIX B



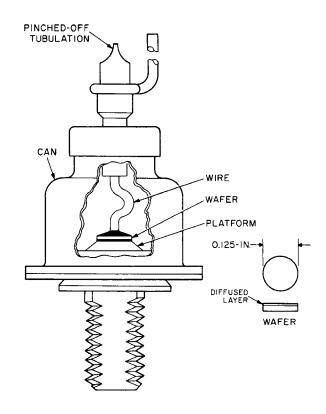
NPN MILLIWATT SILICON DIFFUSED TRANSISTOR - 16 TYPE (PLANAR)

The 16-type transistor is used principally as a general purpose, radio-frequency, small-signal amplifier or high-speed switch.



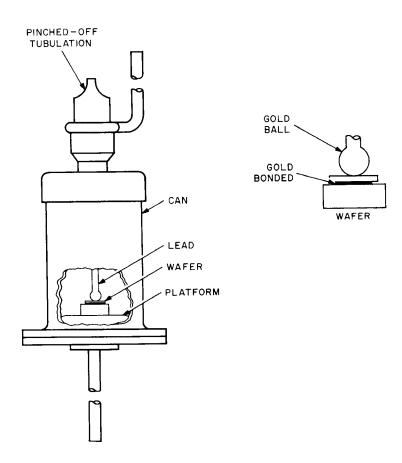
POINT-CONTACT DIODE - 400 TYPE

The 400-type is a general purpose diode used principally as a detector or low-power rectifier. The 441-type diodes are electrically identical to the 400-type, except that they have axial leads.



HIGH POWER SILICON DIFFUSED JUNCTION DIODE - 425 TYPE

The 425-type diode is used principally as a high-power rectifier or voltage regulator, capable of dissipating 10 watts when properly heat-sinked.



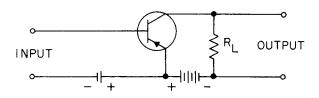
MEDIUM POWER SILICON DIFFUSED JUNCTION DIODE - 426 TYPE

The 426-type diode is used principally as a medium-power rectifier, or voltage regulator.

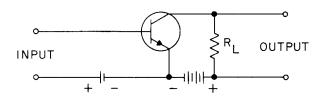
Appendix C

Transistor Circuit Configurations

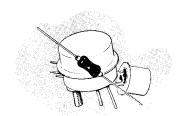
CIRCUIT	CHARACTERISTICS
COMMON BASE (CB)	Lowest input impedance Highest output impedance Low current gain (<1) High voltage gain Moderate power gain
COMMON EMITTER (CE)	Moderate input impedance Moderate output impedance High current gain High voltage gain Highest power gain
COMMON COLLECTOR (CC) (EMITTER FOLLOWER)	Highest input impedance Lowest output impedance High current gain Unity voltage gain Lowest power gain



COMMON EMITTER BIAS CIRCUIT - PNP



COMMON EMITTER BIAS CIRCUIT - NPN



REFERENCE LIST

BASIC THEORY AND APPLICATION OF TRANSISTORS TM 11-690, U. S. Government Printing Office

BELL SYSTEM PRACTICES (Data Sheets)
American Telephone and Telegraph Company

DEFINITIONS OF SEMICONDUCTOR TERMS
Proceedings of I.R.E., Volume 48, October, 1960

HANDBOK OF SEMICONDUCTOR ELECTRONICS Hunter, Lloyd P. McGraw Hill

POWER TRANSISTOR HANDBOOK
Motorola Semiconductor Products Division

TRANSISTOR CIRCUIT DESIGN
Texas Instruments Incorporated

TRANSISTOR MANUAL
General Electric Company

TRANSISTOR MANUAL (Tech. Series SC-10)
R.C.A. Semiconductor and Materials Division

ZENER DIODE HANDBOOK
International Rectifier Corporation